Abstraction Metering Good Practice Manual

R&D Technical Report W84

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**Amendments**
Agency staff wishing to propose corrections or amendments to this manual should do so through the Water Resources Helpdesk.

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## CONTENTS

<table>
<thead>
<tr>
<th>Section</th>
<th>Page</th>
</tr>
</thead>
<tbody>
<tr>
<td>HEALTH AND SAFETY NOTE</td>
<td>(vii)</td>
</tr>
<tr>
<td>GLOSSARY</td>
<td>(ix)</td>
</tr>
<tr>
<td>1. INTRODUCTION</td>
<td>1-1</td>
</tr>
<tr>
<td>1.1 Objectives</td>
<td>1-1</td>
</tr>
<tr>
<td>1.2 The need for abstraction measurement</td>
<td>1-1</td>
</tr>
<tr>
<td>1.3 Requirements for abstraction measurement</td>
<td>1-2</td>
</tr>
<tr>
<td>1.4 Layout of manual</td>
<td>1-3</td>
</tr>
<tr>
<td>1.5 Application of recommendations</td>
<td>1-4</td>
</tr>
<tr>
<td>2. ABSTRACTION CATEGORIES</td>
<td>2-1</td>
</tr>
<tr>
<td>2.1 Summary of statistics</td>
<td>2-1</td>
</tr>
<tr>
<td>2.2 Domestic and Agriculture</td>
<td>2-1</td>
</tr>
<tr>
<td>2.3 Spray &amp; Trickle (Drip) Irrigation</td>
<td>2-2</td>
</tr>
<tr>
<td>2.4 Industrial and Commercial</td>
<td>2-3</td>
</tr>
<tr>
<td>2.5 Electricity Generation</td>
<td>2-4</td>
</tr>
<tr>
<td>2.6 Public Water Supply</td>
<td>2-5</td>
</tr>
<tr>
<td>2.7 Other uses</td>
<td>2-6</td>
</tr>
<tr>
<td>3. GENERAL GUIDANCE</td>
<td>3-7</td>
</tr>
<tr>
<td>3.1 Performance</td>
<td>3-7</td>
</tr>
<tr>
<td>3.2 Meter sizing</td>
<td>3-9</td>
</tr>
<tr>
<td>3.3 Water source</td>
<td>3-9</td>
</tr>
<tr>
<td>3.4 Security of data</td>
<td>3-11</td>
</tr>
<tr>
<td>3.5 Maintenance and checking</td>
<td>3-13</td>
</tr>
<tr>
<td>3.6 Economic factors</td>
<td>3-16</td>
</tr>
<tr>
<td>3.7 Meter inspection</td>
<td>3-16</td>
</tr>
<tr>
<td>3.8 Licence conditions</td>
<td>3-18</td>
</tr>
<tr>
<td>3.9 Current standards</td>
<td>3-18</td>
</tr>
<tr>
<td>4. METERING METHODS</td>
<td>4-1</td>
</tr>
<tr>
<td>4.1 Introduction</td>
<td>4-1</td>
</tr>
<tr>
<td>4.2 Differential pressure methods</td>
<td>4-2</td>
</tr>
<tr>
<td>4.3 Other differential pressure methods</td>
<td>4-5</td>
</tr>
<tr>
<td>4.4 Positive displacement flowmeters</td>
<td>4-6</td>
</tr>
<tr>
<td>4.5 Turbine and jet types</td>
<td>4-8</td>
</tr>
</tbody>
</table>
4.6 Fluid oscillatory types  4-12
4.7 Electromagnetic flowmeters  4-13
4.8 Ultrasonic flowmeters  4-17
4.9 Insertion meters  4-20
4.10 Methods for partially filled pipes  4-24
4.11 Assessment methods  4-25
4.12 Totalisers  4-26
4.13 Summary of characteristics  4-27

5. METER INSTALLATION AND LOCATION  5-1
5.1 Installation  5-1
5.2 Flow conditions  5-7
5.3 Location  5-8

6. FLOW CHECKING AND METER CALIBRATION  6-1
6.1 Introduction  6-1
6.2 In situ methods  6-5
6.3 Laboratory methods  6-15
6.4 Electromagnetic meter verification tools  6-16
6.5 Buried meters  6-17
6.6 Verification of data transmission and recording  6-19
6.7 Remedial action  6-19

REFERENCES AND BIBLIOGRAPHY

APPENDIX A - Flow Conversion Tables
APPENDIX B - Existing Installation Assessment
APPENDIX C - Photographs of Flowmeters and Installations
APPENDIX D - Suppliers of Metering Equipment and Calibration Services

ABSTRACTORS SUMMARY SHEETS

Information for Domestic and Agricultural Licence Holders
Information for Spray Irrigation Licence Holders
Information for Industrial and Commercial Licence Holders (including Electricity Generation)
Information for Public Water Supply Licence Holders

LIST OF TABLES

TABLE 2.1 - BREAKDOWN OF LICENCES 2-1
TABLE 3.1 - PERFORMANCE TYPES FROM WIS 7-03-01 3-20
TABLE 4.1 - APPLICABLE METER TYPES 4-1
TABLE 4.2 - SUMMARY OF MEASUREMENT METHODS IN PART FILLEDPIPES 4-25
TABLE 4.3 - RECOMMENDED TOTALISER PRECISION 4-27
TABLE 4.4 - SUMMARY OF CHARACTERISTICS OF CLOSED PIPE FLOWMETERS 4-28
TABLE 5.1 - SEVERITY OF FLOW DISTURBANCE 5-2
TABLE 5.2 - DISTANCES OF FLOWMETER FROM SOURCES OF DISTURBANCE 5-3
TABLE 5.3 - SUMMARY OF IP RATINGS FROM IEC 529 5-11
TABLE 6.1 - KEY TO METER TYPES IN TABLE 6.2 6-2
TABLE 6.2 - INTERVALS FOR FLOW CHECKING (IN YEARS OF USE) 6-3
TABLE 6.3 - DISTANCES FROM METER WHEN USING AN INSERTION PROBE 6-9
TABLE 6.4 - DISTANCES FROM METER FOR USING A CLAMP-ON 6-11
TABLE 6.5 - FLOW CHECKING WITH A CLAMP-ON ULTRASONIC FLOWMETER 6-12
TABLE 6.6 - REMEDIAL ACTIONS 6-20

LIST OF FIGURES

Figure 1- Pipe dimensions ix
Figure 2- Example of a flowmeter performance graph showing various key points xii
Figure 3- Fully developed velocity profile xiii
Figure 4- Velocity profile downstream of a bend xiii
Figure 3.1 - Example of accuracy expressed as per cent reading and per cent full scale 3-7
Figure 3.2 - Relationship between accuracy and repeatability 3-8
Figure 4.1 - Typical Venturi installation 4-4
Figure 4.2 - Differential pressure transducer 4-5
Figure 4.3 - Variable area flowmeter 4-6
Figure 4.4 - Rotary piston meters 4-7
Figure 4.5 - Typical Woltmann meter 4-8
Figure 4.6 - Typical combination meter 4-10
Figure 4.7 - Irrigation meters 4-11
Figure 4.8 - Fluidic oscillator 4-13
Figure 4.9 - Electromagnetic flowmeter 4-13
Figure 4.10 - Operating principle of an electromagnetic flowmeter 4-14
Figure 4.11 - Earthing an electromagnetic flowmeter 4-16
Figure 4.12 - Ultrasonic Doppler flowmeter 4-17
Figure 4.13 - Transit time ultrasonic flowmeter 4-18
Figure 4.14 - Electromagnetic insertion probe 4-20
Figure 4.15 - Alignment of insertion probes 4-21
Figure 4.16 - Averaging pitot tube 4-24
Figure 4.17 - "Watering can" meter for part filled pipes 4-25
Figure 4.18 - Typical totaliser display 4-27
Figure 5.1 - Poorly fitted gaskets can cause flow disturbance 5-1
Figure 5.2 - Always install electromagnetic meters downstream of pumps 5-2
Figure 5.3 - Bad and good installation practice 5-4
Figure 5.4 - Designs of flow straightener 5-5
Figure 5.5 - Vertical installation 5-5
Figure 5.6 - Installation of electromagnetic and ultrasonic instruments 5-6
Figure 5.7 - Installing the meter to maintain a full pipe 5-6
Figure 5.8 - Suitable and unsuitable meter locations 5-7
Figure 5.9 - Avoid installation in direct sunlight 5-9
Figure 5.10 - Avoid sites where chemical leaks or spillage may occur 5-10
Figure 5.11 - Avoid positions where vibration may be present 5-10
Figure 5.12 - Meter should be supported 5-10
Figure 6.1 - Examples of how to include a transfer standard 6-7
Figure 6.2 - Reservoir drop test 6-8
Figure 6.3 - Testing with an insertion meter 6-10
Figure 6.4 - Thermodynamic method 6-13
Figure 6.5 - Tracer dilution method 6-14
HEALTH AND SAFETY

IMPORTANT NOTE

This manual contains procedures which may have to be applied in hazardous situations. These must be carried out in a safe way in accordance with any appropriate safety procedures. The following have been identified as potential hazards:

- working with electricity
- working near water
- confined spaces
- lone working
- pipelines under pressure
- lifting heavy objects, e.g. drain covers
- chemicals (e.g. tracers or cleaning/disinfection agents).
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GLOSSARY

More complete explanations of some of these terms can be found in the main text. The relevant section number is given in brackets where this is the case.

**Accuracy** - Qualitative assessment of the reading given by an instrument compared to the true value over a defined range of flows (Section 3.1.1).

**Bi-directional** - Measures flow passing through the meter in either direction.

**Bore** - Internal diameter (i.d.) of pipe, see Figure 1.

**Calibration** - Determination of the relationship between flow rate and reading which may include mechanical or electrical adjustments to produce a desired characteristic.

**Cavitation** - Release of gas dissolved in the fluid or vaporisation of the fluid due to the local static pressure dropping below the vapour pressure of the fluid.

Figure 1 - Pipe dimensions
Combination meter - Meter which comprises a main meter, usually a Woltmann type, with a smaller meter mounted in a by-pass, with an integral valve to divert flow through whichever meter is appropriate for the flow rate (Section 4.5.2).

Conductivity - The ability of a fluid to pass an electric current, commonly expressed in micro-Siemens per centimetre (μS/cm).

D (diameter) - Nominal bore (internal diameter) of a pipe, see Figure 1. Multiples of pipe diameters are a useful dimension for specifying pipe lengths, e.g. for the distance between a flowmeter and a fitting.

Differential pressure cell - Device for measuring the difference in pressure between two points (Section 4.2.2).

Electromagnetic flowmeter - Flowmeter which utilises the Faraday effect, i.e. an electromagnetic field is generated across the pipe and the movement of a conductive fluid, e.g. water, through the field causes a voltage to be produced which is measured and used to calculate flow rate (Section 4.7).

Error - Difference between a single measured value and the true value, often expressed as a percentage of the true value.

Flowmeter - Device which measures either the rate at which fluid is flowing past a certain point or which gives the total amount of fluid which has passed a certain point in a known time.

NOTE: In this report, the term flowmeter, or meter, is taken to include the flow sensor and any associated secondary device, electronics or automatic data recording device.

Flow checking (Verification) - Testing whether a meter is reading to the desired accuracy by comparing its readings with those obtained simultaneously by another method or meter of known accuracy.

Flow rate - Quantity of fluid passing a particular point per unit time.

Flow straightener - Device placed in the flow to help recover a fully developed velocity profile (see below) after a source of disturbance (Section 5.1.3).

Full scale - The maximum flow rate that the flowmeter will read to a specified accuracy.

Head loss - A measure of the energy required for the fluid to pass through obstructions and fittings in a pipe, expressed as a drop in pressure.

Helix meter - See Woltmann meter.

Impeller meter - See Woltmann meter.

Insertion flowmeter - Flowmeter which is inserted through the wall of a pipe via a gland (Section 4.9).
In-situ - Without removing the instrument from the pipeline.

Integrator - See Totaliser

Jet meter - Flowmeter where the fluid is forced through one or more small orifices onto the blades of a rotor (Section 4.5.3).

Local or point velocity - The fluid velocity at a discrete point in the flow.

Mean axial velocity - The volumetric flow rate divided by the cross sectional area at the point of measurement.

Multimeter - Instrument for measuring electrical currents and voltages.

National Standard - The National Standard flow rig is at the National Engineering Laboratory (NEL) in East Kilbride. It can trace its measurement of the mass of water passed directly to the National Standard kilogram. By definition, it is the most accurate test rig in the UK against which other rigs should be compared.

Non-intrusive - Meter has no parts intruding into the flow and hence causes minimal disturbance and head loss.

Oscilloscope - Instrument for measuring electrical voltages and displaying the wave form on a screen.

Positive displacement flowmeter - Meter which divides the fluid up into discrete, known quantities (Section 4.4).

Primary device - A device which generates a signal enabling the flow rate to be determined.

Q - Flow rate, often used with a suffix to indicate particular flow rates, see Figure 2:

- $Q_{\text{min}}$ - the minimum flow rate that an instrument can measure to the maximum specified error.
- $Q_{\text{max}}$ - the maximum flow rate at which the flowmeter will operate for short periods of time without deteriorating.
- $Q_t$ - the transitional flow rate, i.e. the rate at which the maximum permissible error changes in value
- $Q_n$ - the nominal flow rate of a flowmeter.

Repeatability - The ability of an instrument to record the same value for the same flow under the same conditions in a short period of time (Section 3.1.3).
**Reproducibility** - The ability of an instrument to record the same value for the same flow over the long term.

**Secondary device** - A device which receives a signal from the primary device and displays, records, converts and/or transmits it as a measure of flow.

**Strainer** - Device placed in the flow to remove weed, gravel and other debris (Section 5.3.5).

**Swirl** - A component of flow which is rotating around the longitudinal axis of a pipe.

**Totaliser** (Integrator) - Device which records the total quantity of liquid to have passed through the meter. This may be integral to the meter or a separate unit (Section 4.12).

**Transfer Standard** - A flowmeter calibrated to a known uncertainty against which another flowmeter can be compared (Section 6.2.1).

![Flowmeter Performance Graph](image)

**Figure 2 - Example of a flowmeter performance graph showing various key points**

**Turbine flowmeter** - Flowmeter that has a rotor mounted in the flow (Section 4.5).

**Turndown** – the turndown of a flowmeter is the ratio of the maximum to minimum flow rates that the instrument can measure within a specified accuracy. (See section 3.1.4).

**Ultrasonic flowmeter** - Flowmeter that operates using pulses of ultrasound (Section 4.8).
Uncertainty - Band around the measured value within which the true value lies with a stated probability, usually 95% (Section 3.1.1).

Uni-directional - Measures flow in one direction only.

Velocity profile (Sometimes referred to as “flow profile”) - The distribution of point velocities over the cross section of the flow. Frictional forces between the flowing fluid and the pipe wall will slow down the fluid close to the wall so that it has a lower velocity there than the centre of the pipe. The operation of the types of flowmeters likely to be used for abstraction purposes assume that the velocity profile on inlet to the meter will be what is known as “fully developed”, see Figure 3. Deviations from this shape caused by bends, Figure 4, valves and other fittings are likely to cause inaccuracies in the flowmeter reading amounting to several per cent.

![Figure 3 - Fully developed velocity profile](image)

![Figure 4 - Velocity profile downstream of a bend](image)

Verification - See Flow checking
**Volumetric flow** - The volume of fluid passing a certain point per unit time.

**Woltmann meter** - Type of turbine meter with a helical rotor (Section 4.5.1).
1. INTRODUCTION

1.1 Objectives

This Manual is intended for use by Environment Agency (the Agency) permitting, environment management and enforcement staff, as well as by abstractors. It covers the measurement by meter of water in closed conduits which has been abstracted under licences administered by the Agency. It does not include open channel measurement methods such as weirs and flumes which are outside the terms of reference for this manual.

The manual has the following main objectives.

- To provide guidelines on abstraction measurement, which are common across all regions of the Agency;
- To instruct Agency permitting, environment management and enforcement staff on good practice for metering water abstraction. This applies both to new applications and to existing installations;
- To provide a reference work for abstractors, manufacturers, fabricators, installers and contractors;
- To recommend appropriate accuracy standards for all types of abstraction measurement; and
- To improve the standard of accuracy of abstraction measurement.

The manual has been compiled using data from many sources, including existing Agency documents, British Standards, site visits, technical books and papers as well as consultation with abstractors, equipment manufacturers, Trading Standards and Agency staff.

Chapters 8 and 9 of the Agency Licensing Manual\(^1\) give details of licence conditions, inspection and enforcement. This manual provides the link between the licence conditions and the practicalities of metering.

1.2 The need for abstraction measurement

The principal reason for measuring the quantity of water abstracted is to allow the Agency to effectively manage this nation’s raw resources. This is done through a system of CAMS (catchment abstraction management strategies) and licensing whereby those that need to take water from a source apply to the Agency for a licence to abstract. The licence will follow the licensing strategy laid out in the CAMS and impose conditions such as the quantity of water allowed to be removed over a certain period or the rate at which it can be taken.

Reliable metering is essential to provide a record of how much water is taken. This enables the Agency to ensure that:
• CAMS accurately balance society’s need for water against that required to maintain a healthy water environment.

• spare resources can be allocated to new abstractors;

• equitable payments for abstraction can be set;

• licence conditions are complied with; and

• it can provide accurate statistical data required by the Department of Environment, Food and Rural Affairs (Defra).

1.3 Requirements for abstraction measurement

The provision and operation of a flow measurement device is the responsibility of the licence holder with the Agency approving the type, size, installation and subsequent calibration.

The flow measurement equipment must meet the needs of both abstractors and the Agency. The main requirements of abstraction metering equipment are summarised below.

Requirements of abstractors

• low purchase and installation cost \[\text{i.e. low cost of ownership}\]

• high reliability and low maintenance cost

• meets the conditions of the licence to the satisfaction of the Agency

• provides appropriate data to satisfy the needs of the abstractor and the Agency

• easy to read

• has a low head loss (for many applications)

• availability of maintenance and repair facilities

Requirements of the Agency

• meets the conditions of the licence

• records flows to an acceptable accuracy

• robust and reliable

• easy to read

• protected from fraud

• ease of inspection of the meter and surrounding fittings
• ease of verifying the recorded flow

Many of these needs are common to both parties though the priorities may be different. Low cost of ownership and minimal interference with flow are probably of greatest importance to most abstractors. Reliability and accuracy are of most immediate importance to the Agency, with ease of access, inspection and verification being the principal needs of enforcement officers.

The metering requirements of each abstraction must be dealt with on an individual basis and are dependent on local site conditions.

This manual gives guidance on the factors which need to be taken in account such as:

• type of meter;
• size of meter;
• location of meter;
• flow rates;
• surrounding pipe layout and orientation;
• water source;
• category of abstraction;
• meter installation;
• security of data and source;
• safety; and
• cost.

1.4 Layout of manual

The main text of the manual is divided into five sections:

• Section 2 - Abstraction Categories - Once abstracted the water is used for various purposes which may be split into a number of categories. Certain features of each category are discussed in the context of metering their abstractions.

• Section 3 - General Guidance - This section is intended to give general guidance on a number of key issues which will affect the selection and operation of a flowmeter used for abstraction metering.
• **Section 4 - Metering Methods** - This section covers all meter types likely to be found monitoring abstractions and discusses their working principles, advantages, disadvantages and applicability to different types of abstraction. It also includes a section on totalisers.

• **Section 5 - Meter Installation and Location** - Poor installation is one of the main causes of flowmeters giving poor readings. This section highlights the key issues and describes good (and bad) practice.

• **Section 6 - Flow Checking and Meter Calibration** - This section describes the options available for carrying out flow checks on a meter in-situ or in a laboratory.

The main text is supported by appendices giving:

• A - Flow conversion factors;

• B - Criteria for site assessments;

• C - Examples of meters and installations; and

• D - Equipment suppliers.

The second part of the manual comprises a number of summary sheets which are specifically aimed at the abstractors. These summarise the requirements of measurement for each category of abstraction, i.e.

• Domestic and Agriculture;

• Spray Irrigation;

• Industrial and Commercial (including Electricity Generation); and

• Public Water Supply.

1.5 **Application of recommendations**

Agency policy and the wording of individual licences will determine to what extent the recommendations are applied on existing and new abstraction sites.

The guidance in this Manual applies to normal circumstances; exceptional or unusual conditions may preclude their use. However, Agency staff will be provided with advice to allow them to make informed decisions in such circumstances.
2. ABSTRACTION CATEGORIES

2.1 Summary of statistics

Before April 2006, there were about 47,000 licences in force, but deregulation of licences for abstraction of less than 20m³/day has reduced this figure to about 20,000. Based on data from 1995-7, Table 2.1 summarises the breakdown between the different categories of abstraction in terms of:

- the quantity of water licensed for each category as a proportion of the total across all Agency regions²;

- the number of licences issued for each category as a proportion of the total across all Agency regions³; and

- the proportion of licences in each category that include a statement requiring a meter to be used³.

Table 2.1 - Breakdown of licences*

<table>
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<th>Proportion of licensed quantity</th>
<th>Proportion of licences</th>
<th>Proportion requiring a meter</th>
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<td>&lt;1%</td>
<td>57.2%</td>
<td>35%</td>
</tr>
<tr>
<td>Spray Irrigation</td>
<td>&lt;1%</td>
<td>24.0%</td>
<td>69%</td>
</tr>
<tr>
<td>Industrial and Commercial</td>
<td>12%</td>
<td>9.9%</td>
<td>62%</td>
</tr>
<tr>
<td>Electricity Generation</td>
<td>36%</td>
<td>0.1%</td>
<td>33%</td>
</tr>
<tr>
<td>Public Water Supply</td>
<td>51%</td>
<td>4.3%</td>
<td>93%</td>
</tr>
<tr>
<td>High Volume Non-consumptive and other</td>
<td>non-consumptive</td>
<td>4.5%</td>
<td>23%</td>
</tr>
</tbody>
</table>

*For further details see References and Bibliography

2.2 Domestic and Agriculture

This covers the metering of abstractions for domestic (household) supplies to individual properties or estates (sometimes referred to as “private water undertakings”) and all
agricultural uses, except for spray irrigation (see Section 2.3). Typical uses in this category are:

- drinking, washing and cooking in houses or small groups of houses, often in remote areas;
- general farm duties;
- nursery use;
- filling a reservoir in winter to meet periods of high demand;
- cleaning dairies, sheds and equipment; and
- stock watering (the major use in this category).

Whilst the quantity of water taken by this category of use is small and rates of abstraction are low as compared with some other categories, it accounts for over half of licences issued. Installations will usually be owned and operated by farmers and others without specialist metering knowledge.

Many licences currently base the abstraction quantity on numerical estimations, for example head of cattle on a specified day of the year or number of houses supplied. This method is far from ideal; it is extremely difficult to verify, making it open to abuse, and provides poor quality data on which to base resource management decisions.

As the majority of these abstractions are small, i.e. pipe sizes ½” to 1½” (15mm to 40mm), and often on remote sites away from mains power, it is predominantly mechanical meters that are used.

An abstractors’ summary data sheet which summarises the requirements for the metering of domestic and agricultural abstractions is included at the end of this manual. Plates 7 and 17 in Appendix C show agricultural installations.

2.3 **Spray & Trickle (Drip) Irrigation**

This covers the metering of abstractions for irrigation purposes, other agricultural uses are covered in Section 2.2.

Spray irrigation is where water is sprayed into the air through fixed or moveable equipment for watering crops and frost protection, on open ground or in a greenhouse;

Abstractions in this category account for around 25% of the number of licences issued. Many abstractors in this category are on the “two-part tariff” system whereby they pay an annual licence charge plus a charge directly linked to the volume of water taken. Clearly, reliable and accurate metering is essential in this case.

There is a high net loss, due to evaporation and transpiration, from spray irrigation, particularly at the most critical times of the year from the point of view of the availability of
the source. In dry summers direct irrigation of any type can have a significant impact on stream flows.

A number of abstractors have reservoirs which are filled when resource is plentiful, e.g. in winter, to ensure a supply when the resource becomes scarce, e.g. when river levels fall to very low levels. The rate at which the reservoir is filled will usually be lower than that which occurs when irrigation equipment is being supplied directly. It is necessary to ensure that if a single meter is being used for both purposes, the range of flow rates are within its specification.

Spray irrigation equipment is often portable as it is used seasonally and may be used for more than one abstraction point and indeed, more than one licence. Similar rules should be applied to both permanent and portable equipment, with particular attention to positioning the meter to achieve an acceptable accuracy and avoiding the possibility of running the irrigation system without the meter in place. Installations for irrigation will usually be owned and operated by farmers and others without specialist metering knowledge.

The majority of meters in the field being used on irrigation are of the Woltmann turbine type. Several variants are available specifically for irrigation purposes. Electromagnetic meters may be appropriate for permanent sites or rotary piston meters for small abstractions.

Currently there are about 15% of such abstractions metered on the basis of pump hours run. This assumes a pump delivery based on the nominal capacity of the pump and is unlikely to be particularly accurate. The measures outlined in Section 4.11 may improve the application of this method but the steps necessary will be impractical or uneconomic for many irrigation installations.

An abstractors’ summary data sheet which summarises the requirements for the metering of spray irrigation abstractions is included at the end of this manual. Plates 13 and 16 in Appendix C show irrigation metering installations.

2.4 Industrial and Commercial

This category includes all abstractions of raw water for use in industrial and commercial applications. Typical uses include:

- evaporative or circulatory cooling;
- general cleaning and washing;
- gravel washing;
- dust suppression;
- process water;
- boiler feed;
- bottling;
• vehicle washing;
• concrete manufacture; and
• brewing.

This is the broadest category in terms of the sizes of installations and uses to which water is put.

Currently there are about 15% of such abstractions metered on the basis of pump hours run. This assumes a pump delivery based on the nominal capacity of the pump and is unlikely to be particularly accurate. Section 4.11 describes how the abstractor may improve on this method but the steps necessary will be impractical or uneconomic for many of the smaller users. Even with the suggested improvements, it is doubtful whether the measurement could meet the required accuracy.

Technical and specialist staff will often be available where the site is owned by a large organisation who will be able to provide the knowledge to ensure that meters are installed, operated and maintained correctly. For smaller organisations these skills may not be readily available.

Despite the broad nature of this category, the majority of meters used will be of the Woltmann turbine type. Industrial abstractors using large amounts of water, e.g. paper mills, will tend to have electromagnetic meters (see section 6).

An abstractors’ summary data sheet which summarises the requirements for the metering of industrial and commercial abstractions is included at the end of this manual. Plates 9, 10, 11, 12 and 18 in Appendix C show metering of industrial abstractions.

2.5 **Electricity Generation**

This section applies to all abstractions for use in electricity generating stations. Typical uses include:

• evaporative or circulatory cooling;
• mixing with ash to make slurry for pumping;
• process water;
• boiler feed; and
• some hydropower generation.

Advice on hydropower developments can be found in the Agency Licensing Manual and ‘Hydropower – a Handbook for Agency staff’\(^1\). Many of these are monitored by open channel installations which are outside the scope of this manual.
Power generators are some of the largest abstractors in terms of volume and account for 36% of the water licensed nationally. However, there are relatively few installations and many only utilise a small proportion of their licence.

Currently there are over half of such abstractions metered on the basis of pump hours run. This assumes a pump delivery based on the nominal capacity of the pump and is unlikely to be particularly accurate. The steps described in Section 4.11 describe how the abstractor may improve on this method but even with the suggested improvements, it is doubtful whether the measurement could meet the required accuracy.

Another surrogate method found in this category is that of using heat transfer and evaporation calculations to deduce the amount of water taken. This has a high level of uncertainty and again will not generally meet the required performance. It is also very difficult to verify due to the number and nature of the variables involved.

Large abstractions such as those in this category need accurate monitoring to manage their impact on the environment. Also the abstraction points are generally large permanent constructions where good installation practice and flowmeter operation should be possible. Technical and specialist staff will usually be available within the organisation owning the site who will be able to provide the knowledge to ensure that meters are installed, operated and maintained correctly.

Many of these abstractions use very large pipework and require a continuous supply, hence insertion meters are commonly used.

The abstractors’ summary data sheet included at the end of this manual for industrial and commercial abstractions includes metering for electricity generation use.

### 2.6 Public Water Supply

This category covers the abstraction of water by water companies for public supply.

This category of use is the largest of those considered, accounting for over half (51%) of the volume of water licensed nationally and a large proportion of the Agency’s income. Licences are often very complex, including multiple abstraction points and sources.

Large abstractions such as those in this category need accurate monitoring to manage their impact on the environment. Also the abstraction points are generally large permanent constructions where good installation and flow metering practice should be possible.

Electromagnetic flowmeters are the most commonly found devices in this category, though many insertion meters are found on larger pipes. Many older installations will have Venturis or other differential pressure flowmeters.

An abstractors’ summary data sheet which summarises the requirements for the metering of public water supply abstractions is included at the end of this manual. Plates 8, 14 and 15 in Appendix C shows metering of a public water supply abstraction.
2.7 Other uses

These are for such purposes as:

- fish farms;
- cress growing;
- amenity;
- recreation;
- fishing pools;
- top-up; and
- hydropower generation. (These are usually monitored by open-channel flow measurement methods that are outside the scope of this manual).
3. GENERAL GUIDANCE

3.1 Performance

3.1.1 Accuracy (uncertainty)

Accuracy is a loosely used term which describes how close the value being displayed by the flowmeter is to the true value. Strictly speaking, what is commonly referred to as accuracy is really inaccuracy. A meter said to have an accuracy of 5% will have an error, i.e. an inaccuracy, of up to 5% and should really be said to have an accuracy of 95%. This report uses the common convention that an accuracy of 5% means an error of up to 5% should be expected.

The accuracy of a flowmeter is usually expressed in per cent either of reading or of full scale deflection (f.s.d.). Figure 3.1 illustrates the difference between these approaches. A meter with an accuracy expressed as x% full scale will have a larger error in proportion to the true value, at flows other than full scale, than one where the accuracy is expressed as x% reading. This becomes increasingly important at low flows.

Note: 1% is chosen as a convenient illustration, it is not intended to be taken as a typical figure.

Figure 3.1 - Example of accuracy expressed as per cent reading and per cent full scale
Accuracy will also be over a defined flow range and different accuracies may be quoted for different ranges of flow. Another important point to note is that the accuracies quoted apply when the meter is installed under ideal conditions (see Section 5.1). Where installation conditions do not meet the requirements specified by the manufacturer, then poorer accuracy will result.

Uncertainty is the statistical expression of accuracy. It is quoted as x% at the y% (usually 95%) confidence level. For example an uncertainty of “5% at the 95% confidence level” means that 95% of the readings taken will be within ±5% of the true value.

### 3.1.2 Acceptable Accuracy

For the majority of abstractions, metering to an uncertainty of ±5% is acceptable. A tighter requirement of ±2% may be considered where the abstraction will potentially have a significant environmental impact, e.g. due to its size or the sensitivity of the source, or where revenue is being collected based directly on the meter reading. However, ±2% will be difficult to achieve for many irrigation abstractions which are on the two-part tariff scheme. Abstractors may meter to a higher accuracy for their own purposes, e.g. process control.

### 3.1.3 Repeatability

Repeatability is the ability of an instrument to give the same reading for the same flow each time. It should not be confused with accuracy. If an instrument has poor repeatability it will have poor accuracy but the converse, i.e. good repeatability means good accuracy is not true. Figure 3.2 illustrates this.

![Figure 3.2 - Relationship between accuracy and repeatability](image)

### 3.1.4 Turndown

The turndown of a flowmeter is the ratio of the maximum to minimum flow rates that the instrument can measure within a specified accuracy. Manufacturers specifications will often quote a maximum flow rate and a turndown from which the minimum flow has to be calculated. For example, a flowmeter with a maximum flow rate of 80 l/s and a turndown of 20:1 will be able to measure a minimum flow rate of 4 l/s.
For meters with electronic analogue outputs, i.e. where the output signal as a voltage or current increases with flow rate (e.g. 0-10 V d.c. or 4-20 mA), the span of the output can usually be set to cover the whole or only a portion of the range between maximum and minimum flows, i.e. the span will not always be equal to the range (turndown) of the instrument.

### 3.2 Meter sizing

The correct sizing of a meter is an important step to obtaining a good measurement. Metering installations should be sized on the rates of flow that the meter will be required to measure, not simply on the diameter of the adjoining pipework. As a rule of thumb, meters should be sized such that the normal operating flow rate is around 60% of the full scale of the meter.

Running a mechanical meter above its full scale flow for an extended period of time will damage it and running at flows below the minimum will give large errors. Most electronic meters, such as electromagnetic or ultrasonic types, will have low and high cut-off points outside of which they will not register. This prevents damage to the electronics at high flows and avoids large errors at low flows.

If the meter has been wrongly sized and is frequently operating near or below the minimum flow that it can record, then under registration of the abstraction will result.

In many cases the bore of the surrounding pipework and of the meter will be the same, however there are reasons for oversizing a pipe:

- to allow for future development of the source;
- to reduce head loss; and
- the installer simply used whatever pipe was available.

In these cases a smaller meter will be required. For good practice, the reduction in diameter should be made at least 5 diameters upstream of the meter with at least 3 diameters downstream before the pipe returns to its original bore (see Section 5.1.2). Reduction and expansion should be via a concentric, tapered adapter and not an abrupt step.

There are abstractors who currently take less water than their licence permits. In these cases consideration must be given as to whether to size a meter for actual flows as seen at present, anticipated flows or licensed flows.

Where there are significant variations in the diurnal patterns of flow, more than one meter may be required to cover the entire flow range. Combination meters (see Section 4.5.2) may be appropriate in these cases, provided the water quality is suitable for such an instrument.

Some pumped abstractions and those gravity fed from a constant head source will tend to have a constant flow.

### 3.3 Water source

Water is abstracted from various sources as set out below.
3.3.1 Water quality

Water quality varies greatly from site to site and can affect the choice of meter type and performance of the meter. There are two aspects to consider:

- solids which are carried in the flow - e.g. grit, sand, weeds, general debris; and
- dissolved material - e.g. minerals, acids.

**Solids**

- Generally surface waters will contain various amounts of solid material whilst underground sources will contain little or no solid matter.

- Some meter types cannot be used with water that contains weeds or other matter and require strainers to be fitted where this may be a problem, see Section 5.3.5. It will not be a problem for non-intrusive types such as full bore electromagnetic or ultrasonic meters.

- Fine sand carried in suspension can be highly abrasive and damage meters. Electromagnetic meters are available with special linings for such cases.

- The presence of organic matter in the source can lead to a build up of slime in pipes and fittings. Regular cleaning is necessary where this is likely to occur.

**Dissolved matter**

- The dissolved content will be more of a problem from underground sources.

- Some electromagnetic flowmeters may perform poorly in waters with very low conductivity (less than 10μS/cm) as may be found in some upland waters.

- Acids washed out from peat can cause corrosion.

- Calcium deposits can build up in pipes and fittings on hard water sources. Regular descaling will be necessary where this occurs.
• Sources rich in iron oxide can be highly corrosive.

• In some special cases, on sources which are highly chemically corrosive, it may be necessary to install the meter downstream of any treatment or purification system.

3.3.2 Sensitivity of source

Consideration should also be given to the environmental importance of the source. Accurate metering will not by itself prevent problems to sensitive water courses, e.g. small brooks drying up, but it will enable officers to ensure that the abstractors are complying with the terms of their licence and provide evidence for prosecution where over abstraction is causing the problem. More stringent accuracy standards and/or more frequent reporting regimes may be considered in particularly sensitive cases.

3.4 Security of data

In order for the Agency to maintain accurate data on abstractions, it is important that the readings generated by a meter are protected from unauthorised tampering. This may be a particular problem for remote sites or sites to which the public have access. One or more means of protection may be needed depending on the site conditions.

Some types of abstraction are particularly open to abuse and the licence holder may have a high motivation to reduce the recorded abstraction. For instance abstraction equipment is often portable, and the flowmeter can easily be removed from the pipeline or bypassed while continuing to abstract. Where the licence is subject to a two part tariff* any reduction in recorded abstraction will result in a lower charge to the licence holder.

Means of protecting the meter reading include:

• non-resettable totalisers;

• mechanical methods, i.e. seals or a locked box;

• electrical interlocks, i.e. a key which needs to be turned in a lock before any changes can be made;

• passwords or security codes for microprocessor based instruments*;

• “blind” devices*, i.e. with no display or keypad, which are programmed and interrogated through a PC, electronic organiser or other device which is removed from site when not required. (This also reduces vandalism.);

• careful choice of the location of the meter, (see Section 5.3);

• specifying that the meter must be an integral part of the portable abstraction pump or the spray head, mounted with either bolted flanges or welded or glued joints, installed and located correctly to ensure accurate measurements (see Section 5);
• provision of seals to indicate tampering or removal of the meter;

• unannounced inspection visits; and

• maintenance of historical trends of the abstraction to enable sudden drops in abstraction to be detected.

* There can be practical and logistical problems with these methods and hence they are less preferable than the other methods.

### 3.4.1 Removable mechanisms

With many mechanical meters it is very easy to change the register or even to remove the internal mechanism unless the parts are sealed. This may be done by having a copper wire linking the register to the meter mechanism and to the meter body, secured with a lead seal. This can be seen in Plate 3 Appendix C. However, the internal parts may need to be removed quite legitimately for cleaning. Whenever, the seal is broken for such purposes the Agency should be informed.

### 3.4.2 Zeroing totalisers

The zeroing of totalisers whenever a reading is taken can be a problem. This must be discouraged and meters with non-resettable totalisers should be used, see also Section 4.12.

### 3.4.3 By-passing the meter

An installation that gives the opportunity to by-pass the meter should be avoided in the majority of situations. However, it is acknowledged that there are exceptional circumstances where a by-pass may be necessary, for example to divert the flow whilst the meter is undergoing maintenance without disrupting the supply. These should be discussed and agreed in writing with the Agency prior to installation.

The integrity of the pipework between source and meter needs to be maintained, i.e. there should be no leaks, and any tappings which may legitimately be present, e.g. to enable in-situ flow checks with an insertion meter, should be capable of being locked off when not in use. The use of glued or welded joints or permanent push fittings offers more security than screwed, snaplock or flanged fittings.

Where by-passes around the meter are legitimately fitted the by-pass should also be metered to the same standard as the main line. The readings from each meter should be recorded separately to facilitate tracing readings back in cases of dispute. By-passes for other purposes, e.g. chemical dosing, should be downstream of the meter.
3.4.4 Loss of power

Many old electronic meters were prone to losing their data or settings when an interruption occurred in their power supply. This does not tend to be a problem with modern meters which will hold their current values when power is removed and resume normal operation when it returns. Where power interruptions may occur on a regular basis and an electronic meter is preferred, a battery powered device should be used or a back up supply provided to ensure that data is not lost. Cabinets with solar power panels are available which provide a top up to batteries.

3.5 Maintenance and checking

3.5.1 Maintenance

Flowmetering equipment requires a certain amount of maintenance. Mechanical meters will require more frequent attention than most electronic types. Electromagnetic and ultrasonic devices should be virtually maintenance free in normal operation, but still need to be checked regularly to ensure that they have not drifted.

Manufacturers will give procedures for maintenance, which should be followed but will often not indicate how often maintenance procedures should be carried out. This will be dependent on local site conditions, particularly the cleanliness of the water passing through the meter. Local site experience and frequent checking when the instrument is first installed will generally be the only means of determining any maintenance interval. Manufacturers may give verbal advice based on their experience with similar installations, which may be helpful.

Closed pipe meters must be kept clean and free from fouling. In many cases cleaning is all that can be performed by the user as any further dismantling can significantly alter the performance characteristics of the meter, i.e. its calibration. Some Woltmann meters are constructed such that the user can remove the rotor and register assembly from the casing, without removing the casing from the line. This facilitates examination of the meter and cleaning but makes the meter open to possible fraud (see Section 3.4.1).

3.5.2 Routine examination

Currently there are no recognised guidelines in the UK for how often a meter should be examined for wear and tear, corrosion or other damage. However, the abstractor should ensure that all equipment is visually examined, as a minimum, at intervals of one quarter to one third those specified in Table 6.2. For example, a mechanical meter on a continuous abstraction of clean water on a highly critical licence should be examined every 6 to 8 months and an electromagnetic meter every 21 to 28 months. Meters used seasonally should be examined at least at the beginning and end of each season.

The set-up parameters on electronic instruments (e.g. positions of dip switches, software parameters) should also be compared with the settings when the meter was installed or last calibrated, whichever is the more recent. Regular comparisons should be made between an instrument’s internal totaliser (where fitted) or the local display and the values recorded by
any logging system or other remote display from which routine readings might be taken, see Section 6.4. Records should be kept of all such examinations.

More frequent examination may be necessary in some cases, e.g. where the meter is installed in a particularly harsh environment. Again manufacturers’ experience and local site experience will be useful in determining an appropriate interval. Examinations should also be made whenever the meter gives a reading which is significantly higher or lower than that which would be expected based on site experience.

3.5.3 Flow checking

The meter should be verified at intervals throughout its life; this is known as flow checking. Mechanical components will wear and the performance of some electronic components will drift with time. Section 6 describes methods of performing flow checks in detail. Calibration of the meter will be required if the flow checks show performance has deteriorated and drifted from the original/factory settings.

It is difficult to specify a precise interval as wear and drift rates will depend greatly on local conditions. Manufacturers may be able to recommend an appropriate interval, given data on the site conditions. However, a note of caution: the manufacturer’s recommended intervals are based on a best case scenario, which may be different from conditions found in the field. Currently there are no recognised guidelines in the UK for the frequency of flow checking a meter but the intervals in Section 6.1 are suggested as minima in the absence of other information, provided the instruments are installed, operated and maintained correctly.

Routine meter examinations and flow checks, i.e. those carried out at the intervals suggested by the manufacturer or this manual, are the responsibility of the abstractor who must bear the cost. Agency officers may also carry out additional tests using one of the methods described in Section 6. This will indicate the accuracy of the meter as installed and reliability of the readings obtained.

3.5.4 Storage

Many meters used in seasonal abstractions, e.g. irrigation, are removed and stored when not in use. With most mechanical meters, it is preferable that they are stored wet, i.e. a blanking flange and gasket should be fitted to one end, the meter filled with clean water and a similar blanking flange and gasket fitted to the other end. Some types may be stored dry, again manufacturer’s instructions should be followed.

Whether the meter is stored wet or dry, the ends should be securely covered to ensure that foreign matter, insects or animals cannot get into the mechanism and cause damage. This also prevents the rotation of lightweight rotors due to air currents which may falsely increase or reduce the meter reading.

Meters should not be stored in places where the temperature will fall below zero, as the water left inside even a drained meter, may freeze and damage the mechanism. Conversely they should not be stored next to sources of direct heat or in very high temperatures, over 50°C, as this will also cause damage.
It is good practice to leave the meter in its original packing until immediately before it is to be installed.

### 3.5.5 Meter failure

Many modern, microprocessor based instruments, developed since, say, 1990, will incorporate self diagnostic routines which are able to check their own operation and give an alarm when fault conditions occur. When available, these systems should be enabled and their alarms logged and acted on as soon as possible. This does not mean that regular, visual examination will not be needed however, as a number of faults can occur which may not be detected by such routines.

If a meter fails completely or gives spurious results which cannot be accounted for by any local conditions or fouling, then the manufacturers recommendations contained in the meter instruction manual should be followed. (Note: before any adjustments are made to the meter, the pipework should be checked for leakage which may be causing suspect readings.) If these fail to rectify the problem, the instrument should be returned to the manufacturer. Manufacturers will often replace the failed meter rather than repair it so it is important to have a record of the meter reading prior to dispatch. For rotary piston meters in particular, repair would not be economic and it will be cheaper in most cases to discard a failed meter and install a new one.

If the licence specifies that a meter must be used for measurement, **it is an offence to continue to abstract** if the meter breaks down. If a breakdown occurs, the abstractor must get the meter repaired or replaced as soon as practicably possible. The Agency should be informed immediately of any meter failures and a period agreed for the abstractor to get the meter replaced or repaired. An assessment of any water taken during this period should be kept, e.g. by monitoring pump hours run and pump capacity.

To minimise inconvenience and disruption to supply, abstractors may consider holding a stand-by meter in stock or entering into a service agreement with their meter supplier which guarantees a replacement meter or repair within the agreed time limit.
3.6 **Economic factors**

The total cost of an installation for abstraction metering may include:

- purchase price of the metering equipment;
- installation costs;
- maintenance (parts and labour) and calibration costs;
- power;
- extra pumping costs through devices with a high head loss; and
- reading costs.

The cost of the meter may only be a small part of the overall cost of an abstraction installation. The costs of constructing a meter chamber, for example, or a long run of cable may be more than the cost of the meter itself.

The costs of maintenance and flow checks are also a significant factor. For example, an electronic meter with low maintenance requirements and a 5 to 7 yearly interval for flow checking may be more expensive to purchase than a mechanical meter. But the cost of the additional maintenance and flow checks over a number of years may far outweigh the difference in the initial purchase prices.

All costs are highly variable and it is difficult to give indicative figures. However, the simplest installation of a small, say 50mm, mechanical meter with no requirement for ancillary equipment or construction of a special chamber may be as low as £200, whilst a meter installation for a large public water supply abstraction may cost upwards of £30,000. Some typical figures for the purchase price of meters are given in Section 4.

3.7 **Meter inspection**

3.7.1 **Licence enforcement**

Licence enforcement and prosecution are covered in the Agency’s National Enforcement and Prosecution Policy and in the Agency’s Operational Instruction 'Water Resources Compliance, Enforcement and Incident Investigation'. The latter replaced Chapter 9 of the Agency Licensing Manual and provides guidance particularly on inspection, gathering evidence and prosecution.

Enforcing meter standards must always begin with an examination of the licence conditions relevant to measurement or assessment of the water abstracted. The wording of this part of the licence can vary, reflecting historical practices and regional variations. The licence is a legally enforceable document and the Agency officers’ course of action will generally be dictated by this wording. Good metering practice will become increasingly self-enforcing as
more licences become time limited. Abstractors will have to demonstrate that they have used water efficiently and have a continued justification of need when applying to renew their time-limited licences. In order to do this, an effective and accurate meter is essential.

### 3.7.2 Meter inspections

During meter inspections or enforcement visits, the enforcement officer should verify the following aspects relating to the condition of the abstraction meter:

- presence of meter;
- serial number of meter;
- manufacturer of meter;
- type and size of meter;
- location of meter;
- installation of the meter;
- condition of meter; and
- records of maintenance, calibration and flow checks.

Appendix B suggests some points to look for in more detail when carrying out a meter assessment and contains a tick box form to assist with this. Once the information has been collected on one visit, it is easier to identify any changes that have been made on a subsequent visit.

The extent of the action required by a failure in metering performance will be judged according to the severity of the incident, the effect on the environment, and the record of the licence holder in following previous guidance. The Operational Instruction (OI) 'Water Resources Compliance, Enforcement and Incident Investigation' contains a guide to the level of follow up action for various offences.

### 3.7.3 Evidence

The collection of evidence is also discussed in the OI. Any evidence to be used in court must be adequately referenced to show it was obtained from a properly executed test, e.g. flow check. The evidence may include:

- printout of flow rates from the reference meter, annotated with time and date, and signature of operator and supervisor;
- photographs (or sketches where not possible) of the equipment configuration;
- calibration certificates for the test equipment;
• qualifications of the person carrying out the test; and

• contemporaneous written records of:
  − dates and times
  − meter readings and flow rates from both the meter under test and the reference meter
  − names of all personnel present on site.

3.8 Licence conditions

The wording on licences varies from extremely simple clauses which may be open to interpretation such as “a meter”, to detailed clauses specifying adequate sizing and location, regular maintenance and flow checking, and acceptable accuracy.

Further guidance on licence conditions is given in the OI on Water Resources Compliance, Enforcement and Incident Investigation. New licences should make reference to meter size, location, maintenance, the need for flow checks and accuracy.

This manual may be used as the basis of the requirements for abstraction metering and provides the link between the licence and the practicalities of metering.

3.9 Current standards

The following published standards available may be applicable to abstraction metering. For the most recent information regarding British and European standards you should visit www.bsonline.bsi-global.com

3.9.1 British and European Standards


BS 5728-2 (ISO4064-2) Measurement of Water Flow in Closed Conduits - defines the performance characteristics of rotary piston, Woltmann and rotary inferential meters used for measuring cold potable water. The standard defines four classes of meter - A, B, C and D - based on the minimum measurable flow rate ($Q_{\text{min}}$). Class D has the lowest $Q_{\text{min}}$ and A the highest.

BS 5728 Parts 3-7 (ISO 7858 Parts 1-3) Measurement of Water Flow in Closed Conduits - defines the performance characteristics of combination meters.

BS EN ISO 6817 - Electromagnetic Flowmeters defines the technology of electromagnetic flowmeters but not their performance.
BS ISO 13359 - Electromagnetic Flowmeters defines the flange to flange lengths of electromagnetic flowmeters.


BS 6174 Specification for Differential Pressure Transmitters with Electrical Outputs

BS 6920 Part 1 Suitability of non-metallic products for use in contact with water intended for human consumption with regard to their effect on the quality of the water.

BS 7405 Guide to the Selection and Application of Flowmeters for the Measurement of Fluid Flow in Closed Conduits - a detailed discussion of all current metering technologies, including those for gas and chemicals. It also contains a detailed section on how to select a meter for a particular purpose.

BS EN 24006 Glossary of terms and symbols for measurement of fluid flow in closed conduits.

BS EN 29104 (ISO 9104) Methods of evaluating the Performance of Electromagnetic Flowmeters for Liquids

BS EN 60529 Degrees of Protection Provided by Enclosures (IP code)

3.9.2 Water Industry Standard

A water industry standard, WIS 7-03-01\(^5\), exists for flowmeters. This primarily covers meters for process control and monitoring applications. For many industrial and public water supply applications, the abstraction will be integrated into the process. The standard defines a number of performance categories for flowmeters (regardless of meter technology) applicable to different applications, see Table 3.1. It also places requirements on the behaviour of meters under various electrical and environmental influences which are common to all types.

The standard is supplemented by a series of two part data sheets. Part 1 is completed by the user and lays out the requirements for the instrument and details about the application. This is then sent to potential suppliers who complete Part 2 where they state whether they can comply with the given specification and give various cost of ownership details.

For closed pipe flowmeters the following data sheets exist:

- electromagnetic flowmeters;
- ultrasonic flowmeters;
- differential pressure flowmeters; and
- insertion flowmeters.

The Standard has found widespread acceptance in the Water Industry and provides a sound basis for the specification of meters to be used for abstraction. Types C and D as defined in
the WIS would be appropriate, though many users may use a higher performance meter for their own purposes.

**Table 3.1 - Performance types from WIS 7-03-01**

<table>
<thead>
<tr>
<th>Type</th>
<th>Uncertainty</th>
<th>Repeatability</th>
</tr>
</thead>
<tbody>
<tr>
<td>Type A</td>
<td>±0.5%</td>
<td>±0.2%</td>
</tr>
<tr>
<td>Type B</td>
<td>±1.0%</td>
<td>±0.25%</td>
</tr>
<tr>
<td>Type C</td>
<td>±2.0%</td>
<td>±0.5%</td>
</tr>
<tr>
<td>Type D</td>
<td>±5.0%</td>
<td>±0.5%</td>
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</tbody>
</table>
4. METERING METHODS

4.1 Introduction

This section is intended to introduce the reader to the types of flowmeter for measuring abstractions. A brief description of each method and its most common variants is given but detailed discussions on operating theory have been deliberately avoided. If the reader wishes to learn more about a particular method, some useful texts are listed in the bibliography at the end of this manual. Photographs and illustrations of different meter types can be found in Appendix C.

The type of meter most suited to a particular application will depend on the site conditions and metering requirements. Five types will cover the majority of applications, as shown in Table 4.1. The other types described here may be found on existing installations or may be considered for particular sites where the alternatives above are not suited.

Table 4.1 - Applicable meter types

<table>
<thead>
<tr>
<th>Abstraction category</th>
<th>Possible meter types</th>
</tr>
</thead>
<tbody>
<tr>
<td>Domestic and Agriculture</td>
<td>Rotary piston</td>
</tr>
<tr>
<td></td>
<td>Turbine</td>
</tr>
<tr>
<td></td>
<td>Electromagnetic</td>
</tr>
<tr>
<td>Spray Irrigation</td>
<td>Rotary piston</td>
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<td>Electromagnetic</td>
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*Insertion meters cannot be regarded as good practice for permanent installation, however it is recognised that there are situations where their use may be necessary. In these cases great care should be taken with the installation and it should be possible to perform an in-situ flow check.
4.2 Differential pressure methods

When a fluid flows through a constriction in a pipe there is an increase in fluid velocity as it passes through the constriction. This causes a corresponding pressure drop across the constriction which is proportional to the square of the fluid velocity.

The differential pressure (d.p.) flowmeter comprises two parts; a constriction to generate the pressure drop and a differential pressure cell to measure it. Many different designs of differential pressure generator have been developed, though only the most commonly found varieties will be discussed here. This family of devices has a long history and much work has been done to optimise their design. The various parts of BS 1042 cover differential pressure devices in some detail and contain design criteria for the differential pressure generator and the positions for measuring the pressure drop to achieve a stated accuracy.

Differential pressure devices have several advantages.

- They are simple, well understood instruments;
- Having no moving parts; they are generally reliable; and
- Their characteristics, including the relationship between differential pressure and flow, are defined by BS 1042.

Their disadvantages include:

- Susceptibility to blockage in the connections to the differential pressure cell leading to frequent maintenance requirements; and
- They have a limited turndown, typically 3:1. This is because they have a square root response to flow rate. With a conventional differential pressure cell having a typical turndown of 10:1, the turndown on flow rate becomes just over 3:1.

Improvements in differential pressure cell design, particularly with regard to the electronics, are extending the turndown somewhat.

4.2.1 Differential pressure generators

The three most common differential pressure generators are the orifice plate, the Venturi tube and the nozzle.

Orifice

The orifice plate (Appendix C Plate 2) at its simplest is a thin steel plate with a hole, usually circular, cut into it. This plate is clamped between two flanges in the pipe which have pressure tappings drilled into them. Performance of the orifice plate is dependent on its edges being sharp and good installation conditions. BS 1042 Part 1 gives a table of the installation requirements in terms of the length of unobstructed, straight lengths required up and downstream of the plate. The values range from 5D (i.e. five times the internal diameter of the pipe) when the orifice is placed downstream of a concentric reducer up to 80D for
conditions where swirl may be generated in the flow. Orifices also introduce a relatively high drop in pressure, known as permanent head loss. They are best suited to clean fluids. With a good installation, the accuracy for an orifice can be as low as 1% of the full scale reading.

**Venturi**

The Venturi tube (see Figure 4.1 and Appendix C Plate 1) overcomes some of the problems associated with the orifice. It comprises a cylindrical inlet section, followed by a convergent section, a cylindrical throat section, and a divergent outlet. The pressure tappings are located just upstream of the entrance to the convergent section and at the throat. As the flow is accelerated gradually in the convergent section and decelerated gradually in the outlet, the permanent head loss is very low.

The Venturi can cope with some solids being carried in the fluid and hence is often found on raw water applications. However, deposits may build up in the throat of the meter which will cause it to over-read, hence regular examination and cleaning is advised. To alleviate possible blockage of the pressure tappings, several may be provided in an annular pattern around the section.

The minimum length of straight pipe required upstream quoted in BS 1042 is 1D and the maximum is 30D. The main disadvantage of the classical Venturi is its length, up to 8 diameters, and hence it is relatively expensive to construct and install. The accuracy for a Venturi tube is generally about 2% full scale.

**Dall tube**

One specific variety of Venturi that is fairly common is the Dall tube. This was produced by George Kent (now ABB Kent-Taylor Ltd.) and is much shorter than the full Venturi, being about two diameters long in total. Despite this, it has an even lower head loss and creates a larger pressure drop, allowing for potentially more accurate measurement.

**Nozzle**

The nozzle has a curved inlet section and is much shorter than the Venturi. Head loss is slightly higher, but again a certain amount of solids can be tolerated. Nozzles have no sharp edges, unlike the simple orifice, which can easily be damaged, and hence retain their calibration characteristics longer. Typical accuracy for a nozzle is about 3% of full scale.
4.2.2 Differential pressure measurement

The differential pressure generated needs to be measured in such a way that it is possible to compute the flow rate. Two pressure tappings are required. One is usually upstream of the constriction and the other at, or very near, the throat (narrowest part) of the constriction. BS 1042 also covers the location of the tapping points for the different types of differential pressure generator. The two pressure measurements may be made separately but are more often made simultaneously in a differential pressure device where the connections from the tappings are connected to either side of the pressure sensing mechanism to obtain their difference directly.

Pressure sensing mechanisms can be divided into three types; manometers, mechanical devices and electrical devices. U-tube manometers are the simplest form of pressure measurement. The disadvantages with them are that they need to be read manually and that variations in conditions, e.g. temperature, can affect their readings. Mechanical types also need to be read manually.

Most measurements are now made with electronic pressure transducers, such as that shown in Figure 4.2. These generally have good accuracy (less than 1% full scale) and repeatability. They give an electrical output which can be logged on a data logger or a chart recorder. Some modern instruments incorporate the square root extraction in the electronics of the differential pressure device such that the output signal is directly proportional to flow rate.
4.3 Other differential pressure methods

4.3.1 Variable area meters

These devices, commonly known as Rotameters, are often used for flow monitoring of clean fluids in pipes up to 50mm diameter. They comprise a vertically mounted, tapered glass or plastic tube in which a float is located, see Figure 4.3. As the flow passes up through the tube the float is lifted. An equilibrium is established between the gravitational force and the lift due to the pressure differential across the float. The position of the float indicates the flow on a scale printed on the outside of the tube which needs to be read manually. Alternatively the float position may be detected magnetically and versions with an electrical output are available. Simple versions of these devices are very cheap. They have a turndown of about 10:1 and accuracy typically in the range 2-3% of full scale.

4.3.2 Target meters

A target meter comprises a flat plate mounted in the flow such that the face of the plate is perpendicular to the direction of flow. This is linked to a spring or other force balancing mechanism such that the resultant force of the pressure acting on the up and downstream faces of the plate, can be measured. This type of device was widely used in the water industry as a waste meter where the hinged plate was mechanically linked to a pen on a chart recorder. Typical accuracy is 5 to 10% full scale.
4.4 Positive displacement flowmeters

The family of positive displacement meters includes some of the most accurate flowmeters with some designs having an uncertainty as low as ±0.2% reading. They work on the principle of dividing the fluid entering the meter into discrete volumes by some mechanical means. There are many variations on the theme; the fluid may be divided up by rotating chambers, sliding vanes, pistons, a nutating disc or shaped gears.

These meters are better suited to clean fluids. Any particles in the fluid may cause the meter to jam, or may abrade the walls of the containing chamber leading to leakage through the meter. They are not affected by the flow conditions at the inlet but may introduce a large permanent head loss. Turndown is typically in the range 10 to 20:1. Positive displacement meters are used to measure flows totalised over a known period, rather than the rate of flow at any instant. They are generally expensive, hence their primary use being fiscal metering of high value products, such as hydrocarbons. They also have a high head loss.

Rotary piston (domestic water meter)

The rotary piston meter, which is widely used in the water industry for metering domestic supplies, also falls into this category. Strictly speaking it is known as a semi-positive displacement meter as there may be a small degree of leakage around the chamber. This is taken into account in its calibration. These meters are suited to small abstractions of clean water, though come in sizes up to 100mm nominal bore, see Figure 4.4.
Key characteristics of the rotary piston meter are:

- Mainly for use on pipes up to 50mm bore, though sizes up to 100mm are available;

- Uncertainty is typically equal to or better than ±2% over a defined range (Q_t to Q_max), reducing to ±5% at low flows (Q_min to Q_t) to meet the performance requirements of BS 5728;

- Typical turndown is 200:1;

- They record the total volume passed on local register but some types may be fitted with an optional electronic pulse output for automatic logging which may also enable rate measurements to be made with appropriate electronics;

- Uni-directional;

- Installation of these meters is straightforward as they require no up or downstream straight lengths;

- Small sizes are relatively cheap (typically £25 to £100 at 1996 prices for sizes of 30mm nominal bore and smaller);

- Some types incorporate internal strainers but external, upstream strainers will be needed to remove gravel, weeds, etc. This also facilitates maintenance and prevents clogging at the inlet to the meter;

- Unsuitable for use on sources with large amounts of debris as maintenance requirements on the strainer become excessive; and

- Most damage to rotary piston meters will cause them to read low.
4.5 **Turbine and jet types**

This family of meter includes all those which have an element mounted in the flow which is caused to rotate by the fluid flowing past it. In the axially mounted turbine, the rotor shaft is parallel to the flow direction with the rotor being concentric to the pipe. In the Pelton wheel type, the shaft and rotor are perpendicular to the flow. In the jet meter, the fluid is passed through one or more orifices before impinging onto the blades of a rotor. All types of turbine meter are best suited to clean water, though certain meters are available for irrigation purposes which are designed to minimise problems with fouling.

More sophisticated turbine meters with electromagnetic pick-off coils to detect the rotation of the rotor are available with accuracies of less than 0.5% and repeatabilities of 0.1%. This makes their use widespread in the petrochemical industry though they are probably too expensive for most abstraction purposes.

Insertion turbine meters are also available and are dealt with below in Section 4.9.

4.5.1 **Woltmann meter**

The simplest form of turbine is known as the Woltmann meter (Figure 4.5 and Appendix C Plate 3). This is also known as the helix or impeller meter. It has a helical rotor which is mechanically coupled to a register on the outside of the pipe via a system of gears and/or magnetic drives. These devices are frequently used by the water industry for metering of flows in the distribution network. They are also widely found on abstractions, particularly in industrial, commercial and agricultural applications.

![Figure 4.5 - Typical Woltmann meter](image)

(Courtesy of Schlumberger)

The advantages of Woltmann meters are:

- They are available in a wide size range, 40mm to 300mm bore;
• Turndown is some 10:1 with an accuracy of ±2% reading. Some types claim a much wider turndown (up to 400:1) though often with reduced accuracy at low flows;

• They are low cost (typically £200 to £300 for a 50mm nominal bore, £300 to £600 for a 100mm nominal bore and £500 to £800 for a 150mm nominal bore, all at 1996 prices);

• They require no external power source, which is a major advantage for remote sites and reduces installation costs;

• In many designs, the rotor and register assembly may be removed from the casing without removing the casing from the line. This facilitates examination of the meter and cleaning, though makes them vulnerable to fraud (see Section 3.4 for precautions to prevent this); and

• Most types may be fitted with a pulse output for automatic data logging (though power will be needed for this).

Performance requirements for Woltmann meters on clean water are defined in BS5728.

They have certain disadvantages.

• They are affected by poor flow conditions, particularly swirl. At least 10 diameters of upstream pipe are required, more if there are valves, pumps or double bends present upstream likely to generate swirl;

• Head loss is relatively high; and

• Problems can occur where the upstream head is too low or fluid velocity is too high and cavitation occurs as the fluid passes through the rotor. Apart from impairing the measurement this can lead to damage of the rotor and bearings.

4.5.2 Combination meter

In order to extend the range on these instruments at low flows, the combination meter was developed. This comprises a Woltmann meter with a rotary piston meter (see Section 4.4) mounted in a bypass across the main turbine (Figure 4.6). Inside the main meter there is a spring loaded valve which opens or closes at a predetermined flow rate. At low flows the valve remains closed and all flow passes through the bypass meter. At a predetermined flow rate the valve opens and flow passes through the main meter. A non-return valve is fitted in the bypass leg. Again this is commonly found in water industry distribution systems and may suit abstractions where a particularly wide range of flows are encountered. It has a high head loss. Note the readings from both registers must be added together to obtain the total volume recorded.
4.5.3 Jet meter

These are devices where the fluid is forced through one or more jets (single or multi-jet meters) which impinge onto a rotor. The rotor is mechanically coupled to a totalising register. Rotors are usually mounted horizontally. These devices are relatively cheap and reliable. They are less sensitive to small particles of dirt in the flow and the velocity profile at the inlet than other turbine types. Size range is typically up to 100mm bore and accuracies of 1% full scale are claimed. Head loss is higher than for a conventional turbine. The performance requirements in BS 5728 also apply to jet meters used on clean water.

4.5.4 Irrigation meters

A number of meters are available specifically designed for irrigation applications. These either have a high by-pass around the rotor, i.e. the rotor does not completely fill the bore of the pipe as it does in a conventional design (Figure 4.7a), or they have a meter mounted in a by-pass with an orifice to force a small proportion of the fluid through the meter (Figure 4.7b). These devices are slightly cheaper than a Woltmann type meter typically £250 to £300 for a 100mm nominal bore instrument and £350 to £450 for a 150mm nominal bore meter at 1996 prices. However, they also tend to have a low performance specification, typically 5%, which may not be good enough in some cases, e.g. on a sensitive source. Generally, these meters are not considered suitable for accurate measurement of an irrigation abstraction.
4.5.5 Summary of key characteristics for turbine meters

The key characteristics for turbine type meters are:

- Jet meters available between 15mm and 50mm nominal bore;
- Woltmann meters available ranging in size from 40mm to 200mm nominal bore;
- Uncertainty is typically equal to or better than ±2% over a defined range \( (Q_t \text{ to } Q_{\text{max}}) \), reducing to 5% at low flows \( (Q_{\text{min}} \text{ to } Q_t) \) to meet the performance requirements of BS 5728;
- Turndowns vary from 10:1 to 400:1 depending on model;
- Do not require a power source;
- Record total volume passed on local register;
- Some types may be fitted with an optional electronic pulse output for automatic logging which may also enable rate measurements to be made with appropriate electronics. (Pulse unit will need power.);
- Some models will measure reverse flows but often with an increased uncertainty (reduced accuracy);
- Usually require a minimum of 10 diameters upstream and 5 diameters of downstream unobstructed straight pipe, see Table 5.2;
• The pipework must be configured such that the meter remains full at all times;

• A strainer is required unless the source is clean. Some models are available with a strainer built into the instrument housing; and

• Unsuitable for use on sources with large amounts of debris as maintenance requirements on the strainer become excessive.

4.6 Fluid oscillatory types

4.6.1 Vortex meters

When a bluff body, i.e. one that is not streamlined with respect to the direction of flow, is placed in a flowing stream, vortices will be shed in a predictable manner from the edges of the body at a frequency which is directly proportional to flow rate.

Vortex meters are suited to all kinds of fluids but in dirty fluids the vortex shedding body may become fouled leading to poor performance or in extreme cases line blockage. For water applications the product of the pipe diameter in meters and the fluid velocity in meters per second, must be greater than 0.03 for vortices to form. (For example, in a 100mm pipe velocity must be greater than 0.3m/s). The accuracy can be better than 1% reading, though 1.5% is more typical, and the turndown can be 15:1 or higher. These devices have a low head loss but are affected by poor flow conditions; 40D of unobstructed straight pipe is needed between the meter and source of severe flow disturbance. Power is required for the sensing elements.

Whilst there is no technical reason for eliminating vortex meters for abstraction applications, it is doubtful whether many would be found in service for this purpose.

4.6.2 Fluidic oscillators

The principle of the fluidic oscillator has been known for some time but it is only recently being exploited as a commercial meter. It depends on the Coanda effect for its operation. This is the tendency for a jet of fluid to attach itself to a solid surface.

The fluidic meter has a chamber with two internal walls at a divergent angle to the direction of flow. The incoming jet of fluid will attach to one of the walls, before it reaches the outlet, a small amount of the fluid is ducted off and fed back to a point near the entry of the jet, see Figure 4.8. This forces the jet onto the opposite wall. With careful design a sustained oscillation is set up with the fluid attaching itself to first one wall and then the other. The frequency with which the changeover occurs is proportional to flow rate.

This type of instrument has a wide turndown and good linearity, hence it being considered as an alternative to the rotary piston meter for domestic supply metering. Accuracy can be 1 to 1.5% reading. It is more suited to clean flows, though the manufacturers claim that a certain amount of grit can be tolerated. Power is required for the sensing elements. As a relatively
new device, there is little experience with its use but it may be possible to use it on small abstractions as an alternative to the rotary piston type.

![Flow around feedback loop forces jet onto other wall](image)

**Figure 4.8 - Fluidic oscillator**

### 4.7 Electromagnetic flowmeters

In recent years electromagnetic flowmeters have established themselves as one of the most widely used types of flowmeter. They are eminently suitable for a wide range of applications in abstraction metering. Examples are shown in Appendix C Plates 4, 5, 14 and 15 and Figure 4.9.

![Electromagnetic flowmeter](image)

**Figure 4.9 - Electromagnetic flowmeter**

*(Courtesy ABB Kent-Taylor Ltd.)*

Their operating principle is based on Faraday’s law of electromagnetic induction. A pair of electromagnetic coils is used to generate a magnetic field perpendicular to the flow direction. A pair of electrodes mounted on the third orthogonal axis, i.e. perpendicular to both the flow direction and the magnetic field, is used to detect the voltage generated when a conductive
fluid flows through the magnetic field, see Figure 4.10. This voltage is proportional to the flow rate.

\[ B = \text{Magnetic flux density} \]
\[ U = \text{Mean axial velocity} \]
\[ V = \text{Induced voltage} \]

**Figure 4.10 - Operating principle of an electromagnetic flowmeter**

The key characteristics of electromagnetic flowmeters are as follows:

- They are available in a wide size range, from less than 1mm bore up to 2.5m. For abstraction, sizes below 50mm bore are unlikely to be economic, unless site conditions render mechanical meters unsuitable;

- Uncertainty of ±1% reading or better over a defined range, increased uncertainty outside this range;

- Instruments are available with turndowns of 1000:1 on mains powered devices, up to 400:1 on battery powered instruments;

- Able to measure both rate of flow and totalised flow;

- Bi-directional - some models can record forward and reverse flows independently or give a net value;

- Most models incorporate an alarm which can be activated when a set flow rate is exceeded;

- They are relatively tolerant of distorted velocity profiles, though to obtain best performance at least 5D straight upstream pipe lengths are needed, see Table 5.2;
They have a negligible head loss;
Having no parts intruding into the flow, they can cope well with dirty fluids and do not require upstream strainers;
The pipework should be configured such that the meter remains full at all times;
Battery powered versions are available for remote sites;
Virtually maintenance free;
Linings can be made from many different materials, including ceramic for fluids carrying highly abrasive particles;
Modern microprocessor based instruments have many options for alarms, totalisers, etc. and programming is secured by a software security code; and
Prices vary considerably from manufacturer to manufacturer and depend on the facilities the instrument has.

Their disadvantages are as follows:
They only work with conductive fluids (typically down to 10\(\mu\)S/cm), usually not a problem with abstractions though some upland waters can have very low conductivity which may lead to poor performance;
Electrodes and earthing rings can become coated by grease or fat leading to poor readings, though this is unlikely in abstraction applications;
They can be expensive in large sizes; and
They require an external power source, though battery powered versions are available for remote locations.

The most common problem with these instruments is failure to obtain a good earthing of the pipework and fluid. This is necessary for referencing the signal to obtain a good measurement. There are two common methods of earthing the fluid. One is by having metal rings clamped between the pipe flange and the flowmeter at both ends. These can be tied to earth with a suitable connection, see Figure 4.11. The second method is to have a third electrode inside the flow tube. The main disadvantage with this latter method is that if the small area of this electrode becomes fouled its effectiveness is reduced and the measurement is impaired.

When installing electromagnetic meters in horizontal pipe runs, they should be mounted such that the electrodes are on the sides of the pipe, not top and bottom where there may be an air gap or silting which will impair the measurement.
1. Mounting in metal pipelines

2. Mounting in lined or plastic pipelines

3. Mounting in a pipe with cathodic protection, the meter must be electrically isolated from the pipe.

**Figure 4.11 - Earthing an electromagnetic flowmeter**
A number of instruments are available with inbuilt mechanisms for cleaning the electrodes if they are to be used in applications where fouling may be severe. Insertion probes are also available and are dealt with in Section 4.9 below.

One manufacturer (Endress and Hauser Ltd.) have produced a version specifically for permanently sited abstractions used for irrigation. This was produced in response to demand from the authorities in France for such a device. It would also be suited to such abstractions in the UK where mains power is available.

4.8 **Ultrasonic flowmeters**

Ultrasonic flowmeters can be divided into two types - Doppler and transit time, also known as time of flight. Broadly speaking, Doppler instruments are better suited to dirty fluids and transit time to cleaner ones.

4.8.1 Doppler

The Doppler flowmeter transmits a pulse of ultrasound into the fluid which is reflected by a particle or gas bubble within the fluid, see Figure 4.12. The returned signal will be at a slightly different frequency to the transmitted one due to the Doppler effect. This frequency shift can be measured and related to the velocity of the particle. Some particulate matter or gas bubbles in the fluid are necessary for successful operation of a Doppler meter.

The meter assumes that the particle is moving at the same rate as the fluid, an assumption which is not true in every case. The spatial distribution of particles within the flow is unknown and hence the velocity of the reflecting particle in terms of the velocity distribution (profile) in the pipe is also unknown. This is partly overcome by the instrument calculating its reading from taking many reflections. Various manufacturers are working on sophisticated signal processing routines to overcome these problems.

Some early Doppler flowmeters did not live up to their claims and gave the method a poor reputation. The modern generation of instruments are far superior to their predecessors. Accuracy can be within ±5% reading in good conditions.

![Figure 4.12 - Ultrasonic Doppler flowmeter](image-url)
4.8.2 Transit time

A transit time meter comprises one or more pairs of transducers mounted such that one in a pair faces upstream and the other downstream, see Figure 4.13. On large pipes, the transducers are mounted on either side of the pipe - the Z configuration - and on smaller ones, to increase the path length, the V configuration is used where the transducers are on the same side of the pipe. For very small sizes, a flow cell arrangement is used with the transducers at either end of a straight section in a flattened U shaped pipe.

Each transducer acts as a receiver and an emitter. Pulses are fired alternately up and downstream. The pulse travelling downstream will be accelerated by the flow and that travelling upstream will be retarded. The difference in time for the two signals to travel the same path is directly proportional to the mean axial velocity of the fluid. Performance of transit time meters is superior to that of Doppler devices, accuracies of less than ±2% are possible in good conditions. Even better accuracy, 1%, is claimed by multi-path instruments which have two or more pairs of transducers.

![Diagram of Transit Time Ultrasonic Flowmeter](https://example.com/diagram.png)

4.8.3 Configurations of ultrasonic flowmeters

Ultrasonic instruments are available in a number of different configurations:

**Spool piece** - Transducers are built into a short flanged length of pipe which is fitted between two flanges in the line. For transit time meters, this configuration gives the highest accuracy as the signal path is precisely known.

**Clamp-on** - Transducers are supplied loose or on a mounting track and the user simply clamps them on to the outside of an existing pipe (Appendix C Plate 6). Clearly this minimises the installation time but care is needed to ensure that all relevant parameters, such as pipe wall thickness and material, are known accurately. These will need to be programmed into the instrument on commissioning. Good coupling between pipe wall and transducer is essential. This is generally achieved using a gel. Portable battery powered versions are available for site survey work, temporary monitoring or flow checking other meters.

**Retro-fit** - Often used in large installations, bosses are attached to the outside of an existing pipe and holes drilled through. The transducers are mounted in the bosses such that their
faces are in contact with the fluid. This is necessary on large installations to avoid excessive attenuation of the ultrasonic signal as it passes through thick pipe walls and travels relatively far through the fluid. Again the signal path length needs to be known accurately.

4.8.4 Summary of characteristics for ultrasonic flowmeters

The key characteristics for ultrasonic flowmeters are:

- Spool piece designs available in sizes up to 3m bore. Size range for clamp-on and retrofit designs virtually unlimited;

- Uncertainty of ±1% reading or better over a defined range for spool piece transit time designs, increased uncertainty outside this range. 2% is achievable with retro-fit designs with careful installation;

- Uncertainty for Doppler types should be 5% or less with careful installation and programming;

- To achieve good accuracy with clamp-on devices, great care must be taken with their installation and programming. Parameters such as the internal pipe bore and pipe wall thickness must be known precisely;

- Single path instruments are susceptible to distortions of the velocity profile which will greatly reduce the measurement accuracy. A minimum of 10 straight upstream diameters are required but this increases up to 40D if there are severe upstream disturbances, see Table 5.2;

- Multi-path transit time meters, i.e. with more than one pair of transducers firing across different chords or diameters, offer greater accuracy but at higher cost. They are far less affected by distorted profiles;

- Being non intrusive devices they have a negligible head loss;

- They are relatively expensive for small sizes but clamp-on’s in particular become more competitive on larger pipes. The typical cost of a single path clamp-on transit time meter is between £3000 and £5000 at 1996 prices;

- Clamp-on and retrofit devices are economically attractive on large pipes where the cost of a full bore meter would be very high;

- On a transit time instrument, flows with a very high amount of solid can attenuate the ultrasonic signal causing it to drop out and the meter to be unable to measure;

- Turndown typically in the range 20:1 to 40:1;

- Able to measure both rate of flow and totalised flow;

- Bi-directional - some models can record forward and reverse flows independently or give a net value;
• Most models incorporate an alarm which can be activated when a set flow rate is exceeded;

• Doppler types do not require upstream strainers as they require particles in the flow for correct operation;

• Transit time types will cope with moderate amounts of solids but a strainer should be fitted if there are significant amounts of debris in the water;

• Clamp on designs do not require any invasion of the pipe. Retro-fit versions can be hot tapped into a full pipe, but better accuracy is achieved if installed while the pipe is empty;

• The pipework should be configured such that the meter remains full at all times;

• Virtually maintenance free; and

• On horizontal pipe runs, the transducers should be on the sides of the pipe not top and bottom where the signal may be attenuated by an air gap or silt.

4.9 **Insertion meters**

4.9.1 **Single point measurement**

An insertion meter is essentially a small flow sensor mounted on a pole which is inserted through a gland into the pipe, see Figure 4.14. This will measure the fluid velocity at the probe tip where the sensor is situated. The two most common operating principles for insertion meters which will be found in water abstractions are electromagnetic and turbine. Vortex and differential pressure insertion meters also exist.

![Figure 4.14 - Electromagnetic insertion probe](http://example.com/em_probe.png) (Courtesy of ABB Kent-Taylor Ltd.)

Alignment of the probe in all directions is important for good measurement. Deviations of more than 5° of the probe tip from the direction of flow (yaw) can introduce significant
errors. Most types have a guide bar to assist alignment. The probe must be installed on a diameter of the pipe, i.e. such that the shaft passes through the geometric centre of the pipe. Figure 4.15 illustrates these points.

![Figure 4.15 - Alignment of insertion probes](image)

Insertion probes are more suited to temporary survey work or flow checking other meters, though occasionally they are found as permanent installations in large bore pipes where a full bore instrument would be very expensive.

These devices measure a local point velocity at the probe head, and can achieve an accuracy of less than 2% for this measurement. The difficulty comes when relating the local point velocity to the overall flow rate. Unless great care is taken to survey the site and traverse the velocity profile on at least two diameters at the point of measurement, it is difficult to achieve an accuracy of less than 5 to 10% on the overall flow rate.
The blockage effect may also be an unknown. The presence of the probe blocking the flow path will cause the velocity of the fluid around it to be higher than in the free stream. On large pipes this effect will be small but as the pipe size decreases, it can become very significant. Some manufacturers allow for blockage in the calibration of the instrument, others do not but may be able to provide the appropriate correction factors if asked.

On a permanent installation, the probe will generally be mounted such that the probe head is either on the centreline of the pipe or on the point of mean velocity (approximately 1/8 D). In the former case the local velocity is higher than the mean velocity and so a factor will need to be applied to the measurement to allow for this. Calculation of this factor will have to take into account the velocity profile and the blockage effect. In the latter case, accurate positioning is far more critical. The velocity profile also changes with flow rate and this should also be taken into account.

4.9.2 Summary of key characteristics of single point insertion probes

The key characteristics of single point insertion flowmeters are:

- Insertion probes come with shaft lengths suitable for insertion into pipe bores up to 5m;
- BS 1042 Part 2 (ISO 3354 and ISO 3966) covers the use of insertion meters for closed pipe flows;
- They should only be used where the cost of a full bore meter is prohibitive and are not normally accepted as a permanent meter;
- They measure the point velocity at the probe tip;
- The uncertainty for a point velocity measurement is typically 2%. However the conversion of this to an overall volumetric flow will reduce the accuracy to 5% at best;
- Turndown is up to 80:1 for turbine types and 100:1 for electromagnetic types;
- Electromagnetic types are bi-directional, differential pressure and turbine types only measure flow in one direction;
- May be hot tapped into existing pipes;
- Sensitive to alignment;
- The pipework should be configured such that the section containing the meter remains full at all times;
- 10D to 50D upstream and 5D downstream of unobstructed, straight lengths are needed, see Table 5.2;
- Turbine types suffer from rapid bearing wear and stall at low flows. They require frequent maintenance;
• Weeds and other filamentous material becoming wrapped around the probe may be a problem on some abstractions; and

• An electromagnetic insertion probe will typically cost around £2500 at 1996 prices.

4.9.3 Multi-point measurement

In order to reduce the effects associated with the velocity profile on insertion meters, there are a number of instruments available which have several sensors mounted at intervals along the probe length. Differential pressure and electromagnetic probes exist in this configuration. The former are known as averaging pitot tubes.

Averaging pitot tubes

The simple pitot is a narrow tube having a hole at the end which faces directly upstream into the flow. The fluid is brought to a rest locally at the tip of the tube and hence the pressure in the tube is the total or stagnation pressure. This is equal to the static pressure in the line plus the dynamic head which is proportional to the square of the fluid velocity. Hence if the static pressure is measured locally, the local fluid velocity can also be found. The averaging pitot has several total pressure tappings along its length to obtain an average total pressure across the entire velocity profile, see Figure 4.16. These devices are more suited to clean fluids, else the holes can become blocked. Typical accuracy is claimed to be ±2% reading in good conditions, with a suitable differential pressure gauge.

Multi-point electromagnetic insertion probes

These devices are new in the UK and only available from one supplier (Flowline Manufacturing Ltd.). They appear to offer some advantages, particularly in large pipes where
they are cheaper to install than a full bore meter. An accuracy of 1% is claimed by the
manufacturer. However, at the time of writing, there is little operational experience in the UK
from which to draw any conclusions. They have been used in the United States with apparent
success.

4.10 Methods for partially filled pipes

Measurement of fluid flow in a partially full closed pipe is difficult to do with any precision
and it is preferable to engineer matters such that either an open channel flow measurement
technique (e.g. weir or flume) can be used or the pipe remains full, see Section 5.1.5 and
Figure 4.17.

![Diagram of "Watering Can" meter for part filled pipes](image)

However a number of devices do exist for measuring the flow in a partially full pipe. These
devices measure the fluid velocity and liquid depth independently and combine this data with
the shape of the pipe to give the total flow.

These devices are available as insertable sensors which are installed in an existing pipe length
or as spool piece meters which clamp between flanges in the conventional manner. Manufacturers of insertable sensors often supply mounting rings or kits to help locate the
sensor in the flow.

The minimum pipe diameter for the use of such devices is typically 200mm, with a minimum
depth requirement of 10% of the diameter. Accuracy is likely to be in the range 5 to 10%
reading.

There are a number of combinations of technology which are possible as shown in Table 3.1.
There is little experience of the use of these meters in the UK, but they are more widely used
in Europe. Indeed in Germany charging on some effluent discharges is based on the readings
from such meters.
Table 4.2 - Summary of measurement methods in part filled pipes

<table>
<thead>
<tr>
<th>Depth measurement</th>
<th>Velocity measurement</th>
</tr>
</thead>
<tbody>
<tr>
<td>Electromagnetic</td>
<td>Electromagnetic</td>
</tr>
<tr>
<td>Hydrostatic</td>
<td>Electromagnetic</td>
</tr>
<tr>
<td>Hydrostatic</td>
<td>Ultrasonic</td>
</tr>
<tr>
<td>Ultrasonic</td>
<td>Ultrasonic</td>
</tr>
<tr>
<td>Ultrasonic</td>
<td>Electromagnetic</td>
</tr>
<tr>
<td>Capacitance</td>
<td>Electromagnetic</td>
</tr>
</tbody>
</table>

4.11 **Assessment methods**

Some licences have conditions requiring measurement or assessment of water abstracted by means other than a meter. Examples include:

- pump (or turbine) hours run at an assumed pumping rate;
- heat transfer and evaporation calculations e.g. electricity generation applications;
- the filling of a container e.g. a storage tank or, in one recorded instance, a road cleaning vehicle;
- a numerical method, e.g. head of cattle; and
- related to the product produced, e.g. “five times the quantity of beer brewed”.

Most of these methods are far from ideal and are not favoured by the Agency. In many cases they will be extremely difficult to verify, making them open to abuse, and provide poor quality data on which to base resource management decisions.

There are a significant number of measurements made on the basis of pump running times. These cases assume a pump delivery based on the nominal capacity of the pump and log the number of hours the pump runs, usually electronically. This is clearly unacceptable as the nominal capacity may be significantly different from the actual operating point.

In order to improve any measurements currently made by this method where it is not feasible to install a flowmeter, the abstractor should keep the following records:

- a characteristic curve showing flow against lift, verified periodically (every 2 years) in-situ;
- a continuous record of suction pressure while the pump is running;
- a continuous record of delivery pressure while the pump is running;
- calculation of lift (i.e. delivery less suction pressure); and
- electronic monitoring of hours run.
From this data, flow rate and volume can be calculated but the uncertainty may be large (10% or more).

The Yatesmeter is a method of flow measurement that measures the pressure and temperature changes of the water across a pump and the power supply to the pump motor. From this data it deduces the flow rate. The manufacturers claim that with good practice and a pump lift of over 25m, uncertainties of better than ±1% can be achieved. With less than 40m lift, the uncertainty of the method increases and is unlikely to meet the requirements for abstraction metering.

4.12 Totalisers

In many situations, the output from a flowmeter will be fed to a totaliser or integrator which may be remote from the meter itself, for example, where the meter is installed in a pit or where access is restricted due to safety considerations. Usually these will have a digital display of the reading but carry very little other information, see Figure 4.18. Units of measurement may sometimes be included.

![Figure 4.18 - Typical totaliser display](image)

It is important to be able to verify that the correct totaliser is being read for the appropriate meter. There may be many, for instance, in the control room of a water treatment works. Hence totaliser should be labelled and it should be possible to verify, by following the cable, that it is connected to the abstraction meter.

Some abstractors in the industrial and power generation fields will have control and data acquisition systems (often called SCADA systems) in place to control and monitor their plant. It may be more convenient to take readings from the computer display on such a system but this does not obviate the need for a dedicated totaliser connected to the meter. The computer generated reading should be regularly verified against the dedicated totaliser. Note that it is the local reading that is acceptable in court.

When used with bi-directional flowmeters, many totalisers are capable of giving total forward flow, total reverse flow or the net flow, i.e. forward minus reverse. For abstraction metering the total forward flow is needed.

The following requirements should be observed:

- Wiring between the meter and the totaliser should be visibly and electrically auditable;
• Mains powered totalisers should be protected from interruptions in the power supply;
• Battery powered totalisers should have a battery life of at least 5 years;
• The totaliser should be non-resettable and sealed against unauthorised tampering;
• It is recommended that the register should be capable of resolving the quantity of water to 0.1%, (one thousandth) or less of the annual licensed quantity, see Table 4.3. For example, if the annual licensed quantity is 80Ml, the register or totaliser shall record in tens of cubic metres (10 000’s of litres) or smaller units;
• The totaliser should not roll over more often than every five years, i.e. it should be able to record 5 times the annual licensed quantity without returning to zero; and
• Readings should be recorded in metric units, e.g. litres or cubic metres.

The last three points should be applied to all totalisers, whether remote or fixed to the meter as in the case of mechanical meters.

**Table 4.3 - Recommended totaliser precision**

<table>
<thead>
<tr>
<th>Annual licensed quantity</th>
<th>Units of measurement</th>
</tr>
</thead>
<tbody>
<tr>
<td>10 to 99 cubic metres</td>
<td>10 litres</td>
</tr>
<tr>
<td>100 to 999 cubic metres</td>
<td>100 litres</td>
</tr>
<tr>
<td>1000 to 9999 cubic metres</td>
<td>1 cubic metre (1000 litres)</td>
</tr>
<tr>
<td>10 000 cubic metres (10 Ml) and above</td>
<td>10 cubic metres</td>
</tr>
</tbody>
</table>

4.13 **Summary of characteristics**

Table 4.4 gives a summary of the characteristics of each type of flowmeter for full pipes. There is considerable variation in each group so a single value is not generally applicable. The relative costs also vary considerably depending on the size, performance required and options specified. The accuracy figures quoted are for good installation conditions.

A list of suppliers is included as Appendix D.
<table>
<thead>
<tr>
<th>Characteristics</th>
<th>Differential pressure</th>
<th>Rotary piston</th>
<th>Woltmann (turbine)</th>
<th>Electromagnetic</th>
<th>Ultrasonic</th>
<th>Insertion</th>
</tr>
</thead>
<tbody>
<tr>
<td>Typical turndown</td>
<td>3:1 to 5:1</td>
<td>200:1+</td>
<td>10:1 to 400:1</td>
<td>10:1 to 100:1</td>
<td>10:1 to 100:1</td>
<td>10:1 to 100:1</td>
</tr>
<tr>
<td>Typical accuracy</td>
<td>1% to 5%</td>
<td>2% to 5%</td>
<td>1% to 5%</td>
<td>0.5% to 2%</td>
<td>2% to 10%</td>
<td>2% to 5%</td>
</tr>
<tr>
<td>Maximum size</td>
<td>2.5 m</td>
<td>100 mm</td>
<td>800mm</td>
<td>2.5m</td>
<td>No limit for clamp-on or retro-fit</td>
<td>5m pipe</td>
</tr>
<tr>
<td>Relative cost</td>
<td>low-medium</td>
<td>low-medium</td>
<td>low-medium</td>
<td>medium-high</td>
<td>medium-high</td>
<td>medium</td>
</tr>
<tr>
<td>Relative head loss</td>
<td>low-medium</td>
<td>medium-high</td>
<td>medium</td>
<td>negligible</td>
<td>negligible</td>
<td>low in large pipes</td>
</tr>
<tr>
<td>Limitations</td>
<td>Affected by flow disturbances</td>
<td>Limited sizes</td>
<td>Affected by flow disturbances</td>
<td>Cost for large sizes</td>
<td>External power needed</td>
<td>Good installation critical</td>
</tr>
<tr>
<td>Advantages</td>
<td>Simple, no moving parts</td>
<td>Wide turndown Defined in BS</td>
<td>No power source needed</td>
<td>No moving parts</td>
<td>Good performance</td>
<td>Cost for large pipes</td>
</tr>
<tr>
<td>Water quality</td>
<td>Clean for orifice Venturi will take some solids</td>
<td>Clean</td>
<td>Mostly clean</td>
<td>Irrigation types will pass some solids</td>
<td>No moving parts</td>
<td>Multi-point devices offer better accuracy</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>Low maintenance</td>
<td>Will pass some solids</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>Cost for large pipes</td>
<td>May foul with weeds</td>
</tr>
</tbody>
</table>
5. METER INSTALLATION AND LOCATION

5.1 Installation

Poor installation is one of the most common causes of flowmeters giving poor performance and large errors. Plates 7 to 18 in Appendix C show some examples of good and bad installations found on abstraction sites.

5.1.1 Handling

Flowmeters are scientific measuring instruments. Accordingly they should be treated and handled with care. They should be protected from physical shocks when being transported and manipulated for installation. Care needs to be taken to protect their mechanism as any damage could affect their operation and accuracy. Electromagnetic meters for large abstractions should be installed under the supervision of a competent professional who will sign off the installation when it is completed satisfactorily.

5.1.2 Up and downstream pipework

Most types of flowmeter (the exceptions being positive displacement and certain jet meters, see Sections 4.4 and 4.5.3) will be affected to some degree by the condition of the flow at their inlet. For accurate operation a fully developed velocity profile is needed. Fittings near the flowmeter, i.e. bends, valves, T’s, strainers, reducers, etc., will adversely affect the performance as they will distort the velocity profile. Upstream fittings will have the greatest effect but in some cases downstream fittings can also influence the meter performance. Poorly aligned joints and gaskets can have a similar effect, see Figure 5.1.

![Poorly fitted gaskets can cause flow disturbance](image)

Figure 5.1 - Poorly fitted gaskets can cause flow disturbance
A meter should never be installed immediately adjacent to a pump and all meters should be on the delivery side of a pump. Installing an electromagnetic flowmeter on the suction side is particularly bad practice, see Figure 5.2, as if a partial vacuum develops, e.g. due to line blockage, the lining can fail and become detached from the casing. This effectively destroys the meter.

![Figure 5.2 - Always install electromagnetic meters downstream of pumps](image)

Manufacturers publish guidelines on the minimum lengths of straight, unobstructed up and downstream pipe (of the same bore as the meter) necessary for accurate operation of their instrument, and these should be observed. Figure 5.3 illustrates these and other points on installation.

Sources of disturbance may be put into groups depending on the severity of the disturbance they introduce, see Table 5.1.

### Table 5.1 - Severity of flow disturbance

<table>
<thead>
<tr>
<th>Severity of disturbance</th>
<th>Possible causes</th>
</tr>
</thead>
<tbody>
<tr>
<td>Low</td>
<td>long radius 90° bend reducer</td>
</tr>
<tr>
<td></td>
<td>clean in-line filter</td>
</tr>
<tr>
<td></td>
<td>fully open gate valve</td>
</tr>
<tr>
<td></td>
<td>fully open full bore ball valve</td>
</tr>
<tr>
<td>Medium</td>
<td>2 bends in the same plane</td>
</tr>
<tr>
<td></td>
<td>elbow</td>
</tr>
<tr>
<td></td>
<td>T piece</td>
</tr>
<tr>
<td></td>
<td>abrupt reduction in pipe diameter</td>
</tr>
<tr>
<td></td>
<td>fully open butterfly valve</td>
</tr>
<tr>
<td>High</td>
<td>2 bends in planes at 90° to each other</td>
</tr>
<tr>
<td></td>
<td>Y type basket strainer</td>
</tr>
<tr>
<td></td>
<td>Pump</td>
</tr>
<tr>
<td></td>
<td>non-return valve</td>
</tr>
<tr>
<td></td>
<td>partially opened valve of any type</td>
</tr>
</tbody>
</table>
Test results have been published by a number of organisations, including WRc and NEL, on the performance of meters under disturbed flow conditions which show that the effect of a disturbance on performance varies considerably from meter to meter, even within a batch of meters using the same operating principle.

However, the guidelines in Table 5.2 have been compiled from a number of sources and should be considered good practice. The lengths should be made up of straight rigid pipe. As the size of the installation becomes larger, it becomes increasingly difficult to achieve these distances. In such cases the abstractor should be able to demonstrate by an in-situ verification that the meter is within the required performance specification.

It is very difficult to predict the behaviour of a meter in conditions outside those recommended by the manufacturer, other than to say the accuracy will probably be impaired. An in-situ flow check would be needed to quantify the effect.

**Table 5.2 - Distances of flowmeter from sources of disturbance**

<table>
<thead>
<tr>
<th>Severity of disturbance</th>
<th>Low</th>
<th>Medium</th>
<th>High</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Upstream D</td>
<td>Downstream D</td>
<td>Upstream D</td>
</tr>
<tr>
<td>Orifice/nozzle (1)</td>
<td>6</td>
<td>5</td>
<td>10</td>
</tr>
<tr>
<td>Venturi</td>
<td>0.5</td>
<td>4</td>
<td>0.5</td>
</tr>
<tr>
<td>Positive displacement</td>
<td>0</td>
<td>0</td>
<td>0</td>
</tr>
<tr>
<td>Turbine</td>
<td>5</td>
<td>3</td>
<td>10</td>
</tr>
<tr>
<td>Electromagnetic</td>
<td>5</td>
<td>2</td>
<td>5</td>
</tr>
<tr>
<td>Single path ultrasonic</td>
<td>5</td>
<td>2</td>
<td>10</td>
</tr>
<tr>
<td>Insertion</td>
<td>10</td>
<td>5</td>
<td>20</td>
</tr>
</tbody>
</table>

Note:

1. Typical figures are given, the exact distance depends on the ratio of the orifice to the full bore (β ratio), see BS 1042 Part 1.
5.1.3 Flow straighteners

Flow straighteners or conditioners will not often be found in abstraction measurement.

A flow straightener is a device which may be inserted into the pipe to remove any distortions in the velocity profile and help to recover a fully developed profile in a much shorter distance than would be taken without the straightener. Several designs are available, for example tube bundle, étoile (vaned) or perforated plate, see Figure 5.4. A short distance, typically 3D for an étoile, 5D for a tube bundle and 10D for a perforated plate, is required between the outlet of a straightener and the inlet of the meter. Certain meter manufacturers also produce proprietary straighteners for use with their, or other manufacturers’, meters.

Many more sophisticated designs are available, often based on a combination of these three basic types, but these tend to be specialist tools found where high accuracy is essential, e.g. certain industrial processes.

All straighteners will introduce a head loss though this is low for tube bundle and étoile types. All designs are prone to blockage if weeds, etc. are present in the flow. Whilst flow
straighteners are useful in some restricted situations, it is usually preferable to engineer the installation with the recommended up and downstream pipe lengths, see Table 5.2.

![Flow Straighteners](image)

<table>
<thead>
<tr>
<th>Design</th>
<th>Length</th>
<th>Thickness</th>
</tr>
</thead>
<tbody>
<tr>
<td>Étoile</td>
<td>3-5D</td>
<td></td>
</tr>
<tr>
<td>Tube bundle</td>
<td>2-3D</td>
<td>≈20mm</td>
</tr>
<tr>
<td>Perforated plate</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

**Figure 5.4 - Designs of flow straightener**

5.1.4 Orientation

The manufacturer’s specification sheet will usually indicate whether the meter can be installed in vertical, horizontal or sloping pipelines. Some types of meter will not function well in vertical pipelines, particularly certain mechanical models where vertical installation will affect the loading on the bearings and lead to increased wear and poor performance. Most non-mechanical meters will function well in vertical installations, see Figure 5.5.

![Vertical Installation](image)

In vertical pipes, it is preferable for the flow to be upwards to minimise the effect of any gas or air bubbles in the water.

**Figure 5.5 - Vertical installation**

In horizontal pipelines, electromagnetic and ultrasonic meters should be installed such that a line drawn between the electrodes or ultrasonic transducers is parallel to the ground, see Figure 5.6. This avoids poor measurements due to air gaps which may be at the top of the pipe or silting at the bottom.
5.1.5 Full pipe

Except for a few particular meters which are specifically designed to be used in part-filled pipes, all meters for closed pipe applications require the pipe to be running full for correct operation. It may be necessary to introduce a local kink or shallow U section in the pipe to achieve this, see Figure 5.7. Particular situations to avoid are at a high point where air will accumulate and on downward or horizontal pipes which are open at the end, see Figure 5.8.

The effect of having a partially filled pipe varies from meter to meter and with the amount of water present in the pipe. Some will fail to register and others will substantially over record.
5.1.6 Provision for flow checking

Provision needs to be made in the installation for the in situ flow checking of the meter. This will require straight lengths of pipe up or downstream of the meter in accordance with the recommendations in Table 5.2. T pieces, valves or tappings, may also be needed depending on the method of checking to be used, see Section 6.2.

5.1.7 Meter isolation

Isolation valves may be fitted up and downstream of a meter (preferably 10D and 5D respectively from the meter) with a drain cock between the meter and the downstream valve, to enable it to be isolated for repair or removal.

5.2 Flow conditions

5.2.1 Flow direction

Most flowmeters will be marked with an arrow indicating the preferred direction of flow. For meters capable of measuring bi-directional flow (i.e. flow in either direction through the meter) this will be the direction of positive flow. Some meters will be damaged by reverse flow and if this is likely to occur, e.g. where water may siphon back through a stopped pump, a non-return or check valve should be fitted. Again manufacturer’s data should indicate whether a particular meter is capable of measuring flow in both directions.

5.2.2 Pulsating flow

Pulsating flows such as those arising from the use of reciprocating pumps, oscillating valves or regulators will cause the majority of flowmeters to over register. Pulsation dampers are
available to minimise the problem but these can introduce significant pressure drops and add to the expense and complexity of an installation.

5.2.3 Available head

Some abstractions rely on low head sources, usually gravity fed. Meters used in such circumstances should have a low head loss themselves. Cavitation can occur in mechanical meters where the upstream head is too low, causing damage to the meter and poor readings.

5.3 Location

5.3.1 Security

The meter should be installed as close to the source as possible (subject to the considerations in Section 5.1.1). This is to minimise the loss of water through unmetered leakage and the possibility of the meter being by-passed. (See Section 6.5).

Where possible, the meter and surrounding pipework should be clearly visible to assist inspection. Where the installation is open to public access this may not be appropriate due to the possibility of vandalism or other unauthorised tampering. (See section 6.5 regarding Buried Meters).

Vandalism on remote sites can be a serious problem. This may be to the meters themselves, pipework or other fittings. Simple precautions against this include making the pipework and meter as unobtrusive and unattractive as possible. Where persistent vandalism occurs, equipment may need to be installed in secure buildings or underground chambers.

5.3.2 Power supply

The availability, or lack, of a local power supply may limit meter choice. Mechanical meters do not require any electrical power supply, drawing the energy needed to drive the meter from the flow itself. However power may be needed if an electrical pulse unit is attached to such a device for automatic reading.

All electronic instruments require a power supply though this may be provided by a battery in some instances. Housings which incorporate solar panels to maintain battery charge are available for use in remote locations. It should be noted that a battery powered meter may lose some of its accuracy compared to the same model powered from a mains supply.

5.3.3 Ambient conditions

The majority of instruments likely to be used for abstraction metering will not be affected by the normal variations in atmospheric pressure, temperature and humidity. However the following points should be considered:

- Condensation in the register of a mechanical meter is sometimes a problem which makes reading difficult, but many meters include an integral wiper to overcome this. Avoiding opening the cover in very cold conditions or direct sunlight can reduce the problem;
• Meters should be protected from frost and freezing during periods of low temperature as this is likely to cause damage. Protection may be provided by:
  – removing and storing the meter (see Section 3.5.4) when not in use,
  – installing the meter in a housing with background heating,
  – lagging,
  – trace heating;

• Electronic equipment generally should not be installed in positions where it is likely to be in direct sunlight for long periods, see Figure 5.9. The temperature inside a sealed box in such circumstances can rise far higher than the ambient air temperature and impair the operation of the electronic circuitry;

Avoid siting in direct sunlight. If a sheltered spot is not readily available a shield should be provided.

Figure 5.9 - Avoid installation in direct sunlight

• Installation in areas where corrosive atmospheres or where the meter may be standing in corrosive liquids should be avoided, Figure 5.10. Corrosion will attack vulnerable parts like electronic connectors, plugs and cables first and is likely to cause a gradual deterioration in performance before total failure;

Figure 5.10 - Avoid sites where chemical leaks or spillage may occur
• IP ratings are used in industry to describe the protection an enclosure has against solid objects and ingress of water. Meters should have the appropriate environmental protection (IP rating) for the conditions where they are installed. IP ratings are defined in the International Standard IEC 529 and summarised in Table 5.3. For equipment installed outdoors, it is likely that a rating of at least IP 65 will be needed, IP 68 in installations where the meter may become submerged. For meters installed indoors or in secondary enclosures, a lesser rating may be sufficient;

• Avoid positions where there is vibration in the pipe. This can cause particular problems with ultrasonic flowmeters, leading to poor measurement. With other types of meter, rubber couplings either side of the meter, at least 5D upstream and 2D downstream, can be used to minimise the effect on the meter, as can be seen in Plate 5 Appendix C;

![Figure 5.11 - Avoid positions where vibration may be present](image)

• The meter should be supported on either side, particularly if plastic pipe is being used, to minimise stresses on the pipe and the likelihood of failure, Figure 5.12; and

![Figure 5.12 - Meter should be supported](image)

• Some sensors may be buried, however this practice is not recommended for abstraction meters as it makes examination of the meter and flow checking very difficult (see section 6.5). If the meter is installed below the level of the ground, it should be in a brick walled chamber with adequate access for reading and inspection and appropriate drainage to prevent the meter becoming submerged. If this occurs, the meter will be difficult to read and is likely to lose accuracy and will eventually fail.
**Table 5.3 - Summary of IP ratings from IEC 529**

The first numeral indicates the degree of protection against solid objects

<table>
<thead>
<tr>
<th>First numeral</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>Not protected</td>
</tr>
<tr>
<td>1</td>
<td>Protected against solid foreign objects of 50mm diameter and greater</td>
</tr>
<tr>
<td>2</td>
<td>Protected against solid foreign objects of 12.5 mm diameter and greater</td>
</tr>
<tr>
<td>3</td>
<td>Protected against solid foreign objects of 2.5 mm diameter and greater</td>
</tr>
<tr>
<td>4</td>
<td>Protected against solid foreign objects of 1.0 mm diameter and greater</td>
</tr>
<tr>
<td>5</td>
<td>Dust shall not penetrate in a quantity to interfere with satisfactory operation of the apparatus or to impair safety</td>
</tr>
<tr>
<td>6</td>
<td>Dust tight</td>
</tr>
</tbody>
</table>

The second numeral indicates the degree of protection against water

<table>
<thead>
<tr>
<th>First numeral</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>Not protected</td>
</tr>
<tr>
<td>1</td>
<td>Protected against vertically falling water drops</td>
</tr>
<tr>
<td>2</td>
<td>Protected against vertically falling water drops when enclosure tilted up to 15°</td>
</tr>
<tr>
<td>3</td>
<td>Protected against spraying water</td>
</tr>
<tr>
<td>4</td>
<td>Protected against splashing water</td>
</tr>
<tr>
<td>5</td>
<td>Protected against water jets</td>
</tr>
<tr>
<td>6</td>
<td>Protected against powerful water jets</td>
</tr>
<tr>
<td>7</td>
<td>Protected against the effects of temporary immersion in water</td>
</tr>
<tr>
<td>8</td>
<td>Protected against the effects of continuous immersion in water at a specified depth</td>
</tr>
</tbody>
</table>
5.3.4 Electrical interference

Overhead power cables, generators, motors or high voltage switch gear may all produce electromagnetic interference (EMI) and/or radio frequency interference (RFI). This may have an adverse affect on any electronic parts of a meter either interfering with the measurement itself or the subsequent processing and transmission of the data. Cables should be routed well away from potential sources of interference and electrically screened to minimise such problems. Recent European legislation\(^6\) means that modern instruments, designed since 1987 say, should not be seriously affected by such interference but with old instruments it was a common problem.

5.3.5 Strainers

Many types of flowmeter, particularly mechanical types, will be damaged or have their measurement seriously impaired by weeds, gravel and other matter which may be found in raw water.

To minimise this problem, one or more of the following methods should be used:

- a screen, basket or rosette fitted to the pipe at the intake to minimise any incursion by large pieces of debris;
- supporting the intake on floats to prevent gravel, etc. being sucked from the bed of the source; or
- fitting an in-line strainer.

The choice of method will depend on local site conditions, such as the nature of the debris, size of abstraction and the equipment which needs protection. There are several implications to fitting a strainer which should be borne in mind which are as follows:

- **Head loss** - Strainers will introduce a permanent head loss, particularly as they fill or become blocked, which will reduce the flow;
- **Flow disturbance** - Some types of strainer, e.g. Y type basket strainers, will distort the velocity profile and hence it is necessary to ensure that there is sufficient length of pipe between the strainer and the meter, see Section 5.1.2; and
- **Maintenance** - Strainers will require emptying and cleaning on a regular basis. Chemically aggressive waters can corrode filters.

Some mechanical meters which have been specifically designed for raw water, particularly for irrigation use, have built in strainers.

If the source always contains large amounts of solid material and debris, then the frequent emptying of a strainer or basket may make mechanical meters uneconomic and a non-intrusive device, e.g. a full bore electromagnetic or ultrasonic meter, will be preferable despite the higher initial purchase price.
5.3.6 Safety

Safety is of critical importance in all installations. Safe access to the meter will be required for reading, maintenance and inspection. There are a number of potential hazards which may be found when installing, inspecting, reading or maintaining a meter which include:

- working with electricity;
- working near water;
- lone working;
- confined spaces;
- lifting heavy objects, e.g. drain covers;
- pipelines under pressure; and
- chemicals (e.g. tracers or cleaning/disinfection agents).

The Health and Safety note at the beginning of this manual gives references to the Agency’s procedures but those of the abstractor should also be consulted and, in cases of difference, the more stringent code applied.

Extra safety precautions may be needed on remote sites to which the public may have access.
6. FLOW CHECKING AND METER CALIBRATION

6.1 Introduction

Most flowmeters will have been calibrated before delivery by the manufacturer. This is to ensure that they are within specification. Electronic meters generally come with a calibration certificate showing the results from the calibration of that particular meter. Other meters, e.g. turbine types, do not come with calibration data but should have a conformance certificate or statement which says that the meter has been tested and is within specification. Meters which do not come with any such assurance are unlikely to meet the requirements for abstraction metering. Abstractors should retain this information for inspection by the Agency.

The manufacturer’s calibration will have been performed on a test rig under ideal installation conditions. This demonstrates the best performance which will be obtained from that meter. The installed performance is not likely to be as good as this and will depend on local site conditions. The way the meter is installed plays a major role in determining the installed accuracy but water quality and local environmental conditions will also have an effect.

The abstractor should ensure that the performance of the meter is checked at intervals throughout its life as mechanical components will wear and the performance of some electronics components will drift with time.

It is difficult to specify a precise interval at which instruments should be flow checked as wear and drift rates will depend greatly on local conditions. Manufacturers may be able to recommend an appropriate interval, given data on the site conditions. Currently there are no recognised guidelines in the UK for the frequency of flow checking a meter but the intervals in Table 6.2 are suggested. These are based on the type of meter, the use, source quality and licence criticality.

**Meter type** - Meters have been grouped depending on the effect that different aspects of water quality are likely to have on their performance. Table 6.1 gives a key to the categories adopted when determining intervals for flow checks.

**Water quality** - The presence of foreign matter in the water will affect the wear on the meter and hence the interval at which it should be checked. Further discussion on water quality can be found in Section 3.3.1. In Table 6.2 *clean water* refers to water which contains no filamentous material, large pieces of debris, gravel or significant quantities of sand. Small amounts of fine sand or silt are acceptable. If grit and weeds are present, the shorter of the two time intervals which may be derived should be applied. It also assumes an average mineral content and acidity. On sites where the source is particularly acidic or rich in minerals the frequency of flow checking and meter examination may need to be increased.

**Duty** - *Continuous* applies where the abstraction is in constant use and the meter is running continuously within its operating range. *Intermittent* applies to situations where the abstraction is stopping and starting, for instance where a header tank or reservoir is being filled. *Seasonal* applies to abstractions where the meter will be taken out of service and put in
store for part of the year, e.g. irrigation. If the abstraction is not used during one particular
year then that year need not be counted when determining the interval for flow checking.

**Licence criticality** - More frequent checking may be required for sources where it is
necessary to maintain a tight monitoring regime, e.g. due to environmental significance or
size, see Section 3.3.2.

### Table 6.1 - Key to meter types in Table 6.2

<table>
<thead>
<tr>
<th>Meter type</th>
<th>Instruments included</th>
</tr>
</thead>
<tbody>
<tr>
<td>A</td>
<td>Rotary piston</td>
</tr>
<tr>
<td></td>
<td>Mechanical turbines (Woltmann, combination, jet and irrigation meters)</td>
</tr>
<tr>
<td></td>
<td>Orifice plates</td>
</tr>
<tr>
<td>B</td>
<td>Insertion probes (electromagnetic, vortex and differential pressure)</td>
</tr>
<tr>
<td></td>
<td>Venturi tubes</td>
</tr>
<tr>
<td></td>
<td>Differential pressure transmitters</td>
</tr>
<tr>
<td></td>
<td>Vortex meters</td>
</tr>
<tr>
<td>C</td>
<td>Electromagnetic flowmeters</td>
</tr>
<tr>
<td></td>
<td>Ultrasonic flowmeters</td>
</tr>
</tbody>
</table>

#### 6.1.1 In situ and laboratory flow checks

Methods for flow checking can be divided into two categories:

- laboratory methods, where the meter is removed from the line and taken to a specialist
  laboratory with a flow test rig; and

- in situ methods which check the meter while it is in place in the line.

Some techniques are more suited to proving the accuracy of flow rate measurements and
some to total volume passed.

In any flow check it is preferable to take a number of points spaced throughout the normal
operating range of the instrument.

It is important that abstractors keep records of all flow checks, in situ and laboratory. These
should include the date of the test, results and the method used.
Table 6.2 - Intervals for flow checking (in years of use)

<table>
<thead>
<tr>
<th>Meter type</th>
<th>Water quality</th>
<th>Duty</th>
<th>Flow check intervals (years)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td>Licence criticality</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>Highly critical</td>
</tr>
<tr>
<td>A</td>
<td>Clean water</td>
<td>Continuous</td>
<td>2</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Intermittent</td>
<td>2</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Seasonal</td>
<td>2</td>
</tr>
<tr>
<td></td>
<td>Water with sand or grit</td>
<td>Continuous</td>
<td>1</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Intermittent</td>
<td>1</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Seasonal</td>
<td>2</td>
</tr>
<tr>
<td></td>
<td>Water with weeds</td>
<td>Continuous</td>
<td>1</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Intermittent</td>
<td>1</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Seasonal</td>
<td>2</td>
</tr>
<tr>
<td>B</td>
<td>Clean water</td>
<td>Continuous</td>
<td>3</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Intermittent</td>
<td>3</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Seasonal</td>
<td>3</td>
</tr>
<tr>
<td></td>
<td>Water with sand or grit</td>
<td>Continuous</td>
<td>3</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Intermittent</td>
<td>2</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Seasonal</td>
<td>2</td>
</tr>
<tr>
<td></td>
<td>Water with weeds</td>
<td>Continuous</td>
<td>2</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Intermittent</td>
<td>2</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Seasonal</td>
<td>3</td>
</tr>
<tr>
<td>C</td>
<td>Clean water</td>
<td>Continuous</td>
<td>3</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Intermittent</td>
<td>3</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Seasonal</td>
<td>3</td>
</tr>
<tr>
<td></td>
<td>Water with sand or grit</td>
<td>Continuous</td>
<td>3</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Intermittent</td>
<td>3</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Seasonal</td>
<td>3</td>
</tr>
<tr>
<td></td>
<td>Water with weeds</td>
<td>Continuous</td>
<td>3</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Intermittent</td>
<td>3</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Seasonal</td>
<td>3</td>
</tr>
</tbody>
</table>

6.1.2 Traceability

If the flow check is to be credible, it must be traceable back to National Standards. This means that the components of the method used to check the meter should themselves have been calibrated against a standard of higher accuracy and so on until the National Standard is reached for each component.

This is not usually a problem with laboratory based methods, but establishing the traceability of an in situ method may be very difficult and in many cases practically impossible.
UKAS is the United Kingdom Accreditation Service and some laboratories are UKAS accredited. This means that their procedures for ensuring the traceability of their test methods have been assessed and approved by an independent body. A directory of accredited laboratories is available from UKAS.

6.1.3 Accuracy of flow checking

It is preferable that the method being used to flow check a meter is more accurate than, or at least as accurate as, the meter being tested. However, for in situ flow checks it is often the case that the method being used is potentially less accurate than the meter it is being used to check, e.g. a clamp-on ultrasonic having an uncertainty of ±5% being used to check a turbine meter with an uncertainty of ±2%. This will only detect any large errors present and errors less than the uncertainty of the reference method may not be picked up. Don’t use a method which is not fit for purpose, i.e. if it cannot detect errors at the level required.

Before a reference method or instrument is used in the field it will be necessary to establish its performance characteristics, i.e. its bias and standard deviation. These may be obtained from laboratory tests on the equipment to be used.

For all in situ flow checks, a number of pairs of readings should be recorded, each pair comprising a reading from the meter and a reading from the reference method taken simultaneously. For good practice some 20 to 30 pairs are needed. This will often be impractical but at least six pairs should always be taken. The difference between each pair should be calculated and the mean of the differences found. This can be expressed as a percentage of the “true” flow as given by the reference method.

For practical purposes the following rules of thumb may be adopted, (note these are based on experience rather than strict statistical rules).

- If the mean difference is less than or equal to the reference method accuracy, the meter is probably within specification;
- If the mean difference is greater than or equal to twice the reference method accuracy, the meter is probably outside specification and requires further investigation; and
- If the mean difference lies between these values, and the method has been applied correctly, then investigation by a more accurate reference method, possibly testing at a laboratory, is needed.

See Table 6.5 for an example using a clamp-on ultrasonic flowmeter.
6.2 **In situ methods**

The advantages of in situ flow checks are:

- minimal disruption to the abstraction;
- installation conditions are taken into account; and
- checks can be undertaken over a longer period of time which may give a more representative result.

The disadvantages are:

- some techniques are inherently less accurate than the meter being checked;
- they will not give the same level of accuracy as a laboratory test;
- it may be difficult to demonstrate traceability; and
- stable flow conditions are needed while the flow check is being performed.

The techniques for in situ flow checks are described below but the choice of method depends on the local site conditions. In order of preference, these may be listed as follows:

1. Reference meter (transfer standard) (see Section 6.2.1)
2. Volumetric methods (see Section 6.2.2)
3. Clamp-on or insertion meters (see Sections 6.2.3 and 6.2.4)
4. Thermodynamic and tracer methods (see Sections 6.2.5 and 6.2.6).

Those mentioned under 4 are the most complicated techniques and require sophisticated equipment, hence they will usually need to be performed by specialist contractors. Compact provers will also not be generally applicable to abstraction meter checking. Contractors offering in situ flow checks are listed in Appendix D.

Before any checks are performed, the following points should be observed:

- the system should be checked for leakage, and any leaks plugged;
- any instrument settings or programming should be inspected to ensure that they are correct;
- for differential pressure devices check tappings and lines are clear; and
- a zero test should be performed on electronic meters, i.e. stop the flow totally, without draining the system, and the flow rate reading should go to zero. Check the valves have fully seated and that there really is zero flow before adjusting, i.e. allow time for the water
to settle. (Zero drift is a common problem on old electromagnetic flowmeters and the zero can usually be adjusted by a potentiometer within the electronics, using guidance from the manufacturer’s instructions.)

6.2.1 Reference meter (transfer standard)

In this method a second meter, of known performance is placed in series with the meter to be tested. There are several ways of achieving this, but it is important to ensure that good installation conditions for the reference meter are provided and that the meters do not interfere with one another, see Figure 6.1. Where the transfer standard is installed in a bypass or in a separate leg, the second and third illustrations, the connecting pipes may be flexible but they should be kept as short as possible and the pipework attached directly to the reference meter must be rigid. The transfer standard meter must also be of a type appropriate to the water quality and site conditions. A means of showing that there is no leakage past the valves isolating the main pipe (those marked with a ∗ in Figure 6.1) is also useful. This may be done by using double block and bleed type valves.

Advantages include:

- accuracy better than (or at least as good as) the meter under test;
- method can be made traceable by using a meter, preferably with its own dedicated sections of up and downstream pipework, that has been traceably calibrated at a laboratory;
- any fluctuations in flow will be seen by both meters; and
- this method may be used for either flow rate or total volume passed tests.

Disadvantages include:

- there will usually be some disruption to the supply of abstracted water unless the facility for doing the tests has been engineered into the installation;
- application may be difficult with large meters, > 300mm;
- there may not be a pipe length near the meter of sufficient length in which to fit the transfer standard; and
- the user would need to have a large number of similarly sized meters to make keeping a transfer standard economical.

Clamp-on and insertion meters cannot be regarded as transfer standards, unless they can be installed in a repeatable fashion on a length of pipe in which they have been calibrated.
Flanged section in main line to accommodate transfer standard

Flanged section in by-pass leg

Transfer standard in separate line

Distances A, B and C from Section 5.1

Figure 6.1 - Examples of how to include a transfer standard
6.2.2 Volumetric methods and drop tests

The volumetric method is straightforward in concept though often difficult to engineer in the field, except for small size meters. Water passed through the meter is diverted into a tank or reservoir of known volume. The quantity collected can be compared to that recorded by the meter.

Drop tests are a similar idea, though in this case the water is collected and then passed through the meter, see Figure 6.2. This technique may be possible where water is abstracted and stored in a reservoir or large constant head tank prior to use. To perform the check, the supply to the reservoir is cut off and the water stored allowed to flow out and through the meter. The quantity passed can be calculated by the drop in level and the cross sectional area of the reservoir and compared to the meter reading.

This method is used to determine the total volume passed through any size of pipe. It is particularly useful on small sizes of pipe, e.g. domestic or agricultural abstractions with a ½” to 1½” (15 to 40mm) line, where the volume collected may be relatively small.

Accuracy can be high, 1% or better where the dimensions of the reservoir can be precisely established, but this becomes less easy as the size of the reservoir needed increases or on site, rather than mobile, facilities are used. In the latter cases, an accuracy of 5% is more likely.

![Figure 6.2 - Reservoir drop test](image)

Total volume through meter = \( Ah \) m³
Average rate of flow through meter = \( Ah/t \) m³/s

where \( t \) is the time taken in seconds for the surface to drop distance \( h \) metres
Problems include:

- on large abstractions, having a sufficiently large volume into which the flow can be diverted, or drawn from, to obtain a representative reading;

- supply from the abstraction will be interrupted whilst the test is performed; and

- establishing traceability. For a mobile facility it is straightforward to calibrate the reservoir being used but it is more difficult when using existing on-site facilities as another link in the chain of traceability is needed to establish the precise dimensions of the facility.

### 6.2.3 Insertion meter

Insertion meters are discussed above in Section 4.9 and similar caveats apply to their use for testing as for permanent installations. To use an insertion meter for flow checking it is necessary to have an appropriate tapping in the meter line. This should be sufficiently far from any fittings to ensure good flow conditions, see Section 5.1, and from the meter under test to ensure that they do not interfere with one another; recommended distances are listed in Table 6.3.

<table>
<thead>
<tr>
<th>Type of meter under test</th>
<th>Minimum distance between test meter and downstream insertion probe</th>
</tr>
</thead>
<tbody>
<tr>
<td>Woltmann, jet</td>
<td>20D</td>
</tr>
<tr>
<td>Insertion, positive displacement, orifice, nozzle, Venturi</td>
<td>10D</td>
</tr>
<tr>
<td>Full bore electromagnetic, ultrasonic</td>
<td>5D</td>
</tr>
</tbody>
</table>

Traverses across the pipe should be performed on at least one diameter, and preferably also on a second diameter at right angles to the first, to establish the velocity profile. A stable flow is necessary when traverses are being performed as the velocity profile changes with flow rate. The velocities across the profile can be integrated to give the total flow. Once a profile has been established, and as long as the flow rate remains constant, the probe may be left at a certain position, e.g. at the point of mean flow. Figure 6.3 illustrates this method.
Total flow rate \((Q)\) through the meter equals the sum of the average velocity for each annulus \((V_n)\) multiplied by the cross sectional area of that annulus \((A_n)\).

\[
Q = \sum A_n V_n
\]

**Figure 6.3 - Testing with an insertion meter**

BS 1042 Part 2 gives further guidance on the use of velocity area methods in closed pipes.

This technique is best suited to larger pipes, \(> 200\text{mm}\). On smaller pipes the effects of the blockage due to the presence of the probe become very significant.

This method may be used for rate or total volume passed tests. Traceability of the probe velocity measurement in a certain pipe or tow tank is possible, but it is difficult to make the volumetric measurement required in the field traceable. Accuracy is likely to be 5% at best.

### 6.2.4 Clamp-on meter

There are several portable clamp-on ultrasonic flowmeters available for site survey work which offer a quick and reasonably straightforward means to flow check a meter. Plate 6 Appendix C shows a portable clamp-on meter in use. The use of such devices has been discussed above in Section 4.8 and similar considerations apply to their use as meter testing tools as for permanent installations:

- The instrument must be programmed with the correct data, for example on internal pipe dimensions and materials;
- A fully developed velocity profile is needed for good results, i.e. the distances given in Section 5.1.2 should be observed;
• The pipe must be running full;

• If the clamp-on is being used downstream of the meter under test, the distances in Table 6.4 should also be observed to minimise any flow disturbance caused by the meter;

• Good acoustic coupling is needed between the pipe wall and the transducer. This is achieved by cleaning the pipe and using a coupling gel; and

• Doppler types require some particulate matter or gas to be entrained in the flow for their operation. Transit time devices can cope with moderate amounts of material in the flow.

**Table 6.4 - Distances from meter for using a clamp-on**

<table>
<thead>
<tr>
<th>Type of meter under test</th>
<th>Minimum distance between test meter and downstream clamp-on</th>
</tr>
</thead>
<tbody>
<tr>
<td>Helix, jet, combination, positive displacement</td>
<td>40D</td>
</tr>
<tr>
<td>Insertion, vortex, orifice, nozzle, Venturi</td>
<td>10D</td>
</tr>
<tr>
<td>Full bore electromagnetic, ultrasonic</td>
<td>5D</td>
</tr>
</tbody>
</table>

As a clamp-on device does not itself introduce any flow disturbance it may be installed upstream of the meter to be tested, allowing 5D between it and the meter, provided there is sufficient distance between it and any disturbance further upstream.

The main impairment to the measurement being made traceable is the difficulty in establishing precise data on the pipe, particularly those aspects which may not be obvious from the outside, e.g. internal diameter, wall thickness.

This method may be used for flow rate or total volume passed tests. Clamp-on meters may be used on pipes from 15mm to 2m and over in diameter.

The accuracy of the method very much depends on local site conditions. With good, clean pipe of known dimensions, away from sources of flow disturbance, an accuracy of better than 5% may be obtained. However, as the conditions become less good, i.e. the dimensions of the pipe are less precisely known or there are sources of flow disturbance nearby, the accuracy deteriorates. For example, good results can be obtained for many spray irrigation applications where there are long lengths of regular aluminium pipework on which to clamp the meter. On old cast iron pipes, which may have considerable internal corrosion, clamp-on meters will not give good results.
Many modern instruments include an indication of the strength or the quality of the received signal which can be a useful guide on the quality of the results. Low strength or noisy received signals will not tend to yield reliable results.

The rules of thumb described above in Section 6.1.3 may be applied to flow checks with clamp-on meters as shown in Table 6.5.

**Table 6.5 - Flow checking with a clamp-on ultrasonic flowmeter**

<table>
<thead>
<tr>
<th>Mean difference</th>
<th>Result and possible courses of action</th>
</tr>
</thead>
</table>
| ≤5 %            | Meter under test probably within specification  
                  No action needed |
| 5% < difference < 10% | Check set up of clamp-on, transducer installation and programmed data, and repeat test  
                          If possible use another method to corroborate the results or a “better” site for the clamp-on  
                          Is the installation of the meter satisfactory, if not suggest improvement, e.g. resiting, and check again when done  
                          Is there anything visibly wrong with the meter, e.g. jerky register, physical damage, which may indicate failure? If so meter should be repaired or replaced  
                          If the meter appears sound, is installed correctly and there is no possibility of using another in situ method, the meter will have to be tested at a laboratory. |
| ≥ 10%           | Probably a fault with the meter under test, check set up of clamp on first and repeat test to confirm  
                          Severe flow disturbance*, e.g. a pump very close by, could cause errors of this magnitude, particularly at low flows. If installation is very poor and meter appears sound, suggest resiting, and check again when done  
                          Otherwise, meter should be repaired or replaced. |

* Those listed under “High” in Table 5.1.

6.2.5 Thermodynamic method

As mentioned in Section 4.11, it is possible to infer the flow rate from measurements of the temperature and pressure differences across a pump and the power supplied. Pump efficiency curves are also needed in some cases. To use this method a lift of at least 25m is needed. This is a technique requiring specialist equipment and expertise and will only be applicable to a limited number of sites. The number of variables involved, including the installation of the probes, make achieving traceability to National Standards by this method difficult. Figure 6.4 illustrates the method.
6.2.6 Tracers

This technique is more commonly used in open channels and rivers but can also be applied to closed pipe measurements. There are two variations on this method, dilution gauging and transit time. In each case, a substance, with a certain property which enables it to be distinguished from the water, is injected into the pipe and detected at a second point downstream.

In the transit time method, a short dose is injected and the time taken for it to travel from the injection point to the detection point is measured and used to compute the mean fluid velocity.

In the dilution method see Figure 6.5, a known concentration of tracer is injected in at a known flow rate. Samples are then taken at the detection point and the tracer concentration is measured. By using a ratio of the injected and final concentrations and knowing the injection rate, the total flow rate can be determined. Samples are also taken upstream of the injection point to determine any background levels of the tracer or similar substances which would interfere with the measurement.
BS 5857 describes each of these techniques.

There are practical problems when using this method in the field including:

- access to a sufficient length of pipe (200D or more) between injection and detection points;
- obtaining a stable flow;
- variations in background levels of the tracer or similar substances which may interfere with the detected values;
- the time delays and costs associated with the laboratory methods which are required to determine the resultant low levels of tracer concentration in the final sample; and
- the number of variables involved, including the sampling locations and procedures, make achieving traceability by this method difficult.

This technique determines flow rate and cannot be used for total volume passed. Accuracy at best is likely to be 3%, but is more likely to be worse than 5%.
6.2.7 Compact prover

Provers are most often used in the oil and chemical industries. They are smaller versions of the prover loop described below (Section 6.3). The compact prover is often mounted on a trailer. Even though it measures the time taken to pass a known volume, the volumes and times involved are so low that it is really a test for flow rate measurement. This method is highly accurate, better than 1%, and traceable. Typically, meters up to 100mm may be tested by this method. The main barrier to its use for abstraction meters is the lack of availability of appropriate equipment.

6.3 Laboratory methods

The advantages of laboratory based flow checks are:

- good traceability;
- enable meter to be tested over its full range;
- generally more accurate than in situ checks; and
- provide data that is comparable with the original manufacturer’s calibration.

The disadvantages are:

- likely to be more expensive than an in situ flow check;
- cost of removing, transporting and reinstalling meter;
- takes no account of the installation conditions;
- the disturbance caused by removal of the meter may change its characteristics, for example a piece of debris which had been trapped in the meter causing it to read incorrectly may become dislodged so that when the meter is tested, it will work correctly; and
- disruption to the supply on continuous abstractions.

There are a number of organisations which have facilities for meter calibration and flow checking. These are listed in Appendix D.

The meter is installed on a purpose built rig where flow rates and fluid conditions can be closely monitored and controlled. A quantity of water will be passed through the meter and measured by one of several methods. These include:

- weigh tank (collection of a known mass of water in a measured time);
- volumetric flask (collection of a known volume of water in a measured time);
- calibrated high accuracy reference meter, also known as a transfer standard (usually a positive displacement, high accuracy turbine or electromagnetic type);
- prover loop (this comprises a section of pipe of known volume in which a tightly fitting sphere or piston is mounted; the flow pushes the sphere or piston through the pipe and its
time of travel between two set points at the inlet and outlet of the known volume section is measured.; and

- tow tank tests for insertion probes (the probe is towed along immersed in a tank of water at a known velocity).

Results may be expressed in a number of ways:

- as flow rate measurements;
- in terms of total volume passed; or
- for electronic outputs, as a meter factor, i.e. the average number of pulses per unit volume passed. These must be compared with the factor set in the counter to determine error.

Pressure instrumentation may also be calibrated in a laboratory, either by dead weight testers or against a pre-calibrated reference gauge.

### 6.4 Electromagnetic meter verification tools

**Important note:** the use of an electronic verification tool by itself does not demonstrate the accuracy of the flow measurement; it simply confirms that the components of the meter are working to set specifications. Certificates from such tools should not be accepted without accompanying data from a flow check carried out by a method that directly measures the flow, such as those described in the preceding sections.

A number of the manufacturers of electromagnetic flowmeters offer electronic verification tools that can check the operation of their own flowmeters. Provided that the installation of the meter is acceptable, verification tools may be used to significantly extend the periods between recalibration of the meter.

Each manufacturer’s tool comprises an electronic unit that connects to the flowmeter via its transmitter. Each tool works in a slightly different way but they all run a series of diagnostic electronic tests on different aspects of the flowmeter, including the integrity of the sensor, the transmitter and the connecting cables. They check that the important components of the meter are still functioning as they should. The results are stored and can be uploaded to a computer with the appropriate software (each manufacturer provides bespoke packages for their tool). A table showing the results of the test is produced which can be printed as a test certificate. If all of the results are within pre-set limits, the meter will be passed. However, if any of the results have moved outside those limits then the meter will be failed.

As with all other verification techniques, it is important that any individual using a verification tool shall have been trained and is competent in its use.

The results from verification tests can also be compared with the results from previous tests on the meter and, if available, a set of equivalent results from the meter at the time of manufacture (known as the “fingerprint”). This enables trends to be observed and an early diagnosis of problems before failure occurs.

It is important to remember that such tools:
• do NOT make an independent measurement of the actual flow through the flowmeter and hence cannot be used to calibrate flowmeters;

• will not detect flow measurement errors due to flow disturbance effects or incorrect meter installation or set up (e.g. outputs incorrectly ranged);

• may not detect all faults, particularly intermittent faults;

• do not check the onward measurement chain from the meter, i.e. any telemetry, SCADA or other system from which reported abstraction figures may be taken.

However, they do provide a quick, convenient and reasonably reliable means of checking that a meter is still working. Hence there is growing use of them by water companies for checking abstraction and other meters, particularly where the meter sensor is buried or otherwise difficult to access.

The certificate from a verification tool does not by itself prove the accuracy of the flow measurement being made by that meter. The meter must have been installed by a competent practitioner who will sign to say that it is working to an uncertainty commensurate with the manufacturer’s claims.

Another important point to note is that as these tools run through their test procedures, they exercise the meter outputs over their range and hence will increase the total recorded flow shown on any connected totaliser and the meter display itself. This increase will not correspond to the volume of water passed through the meter during the test.

With at least one manufacturer’s equipment, it is possible to reset the totaliser to the value prior to the test using another piece of software. With another manufacturer’s product, the before and after totals are shown on the certificate. A resettable totaliser is not an acceptable device for recording actual abstracted quantities.

Meter verification tools are distinct from the flow simulators that many manufacturers offer. Flow simulators also plug into the meter transmitter, often in place of the cables to the flow sensor and provide a simulation of the signal that would be coming from the sensor to the transmitter under pre-set flow conditions. They allow the output from the flowmeter to be set up and telemetry links checked under known, simulated flow-rates. Simulators do not generally carry out any checks on the flowmeter. These are not acceptable results as evidence of abstracted quantities.

### 6.5 Buried meters

The burial of metering equipment is not recommended due to the risk of buried meters going wrong and the difficulties associated with maintenance and compliance checking.

It is accepted, however, that some flowmeters can be buried if they are used in conjunction with a verification tool and are subject to all of the following conditions:
6.5.1 Installation and set up

i. The installation of the meter should be audited by a competent individual prior to being buried by checking the size and serial number of the meter and that the up and downstream distances comply with the requirements for that meter and that it is set up in accordance with this good practice guide.

ii. Installation drawings should be made available and inspected to ensure that they are consistent with the actual installation.

iii. The terminals where the meter transmitter cables join the meter sensor should be potted (filled with an epoxy resin or other sealant), cable glands must be tight and there should be no joins in any buried section of cable.

iv. The meter should be tested for accuracy of flow measurement in situ prior to being buried.

v. The set up of the meter transmitter should be verified to ensure that the meter size, flow range etc. are correctly set.

6.5.2 Meter checks and verification

i. The meter must pass annual verification tests, using an electronic verification tool (see section 6.4) in order to continue to be considered satisfactory. Test results will be considered acceptable only if;

a. the checks have been carried out by an operator who has been certified as competent by the meter or verification tool manufacturer and,

b. the initial installation of the meter has been agreed as acceptable by a competent Agency officer.

ii. Periodic flow checks should still be carried out. This may be on an exposed section up or downstream of the meter, though account would need to be taken of any in- or outflows between the point of the flow check and the meter. If such a location is not available, the possibility of cross-referencing readings should be considered, for example comparing abstraction records with works output.

6.5.3 Records

i. Copies of annual verification checks (verification test certificates) must be sent to the Agency with the annual abstraction returns. All checks using verification tools or other methods must be kept and be available for inspection.

It should be noted that some water companies have had to dig up their buried meters due to irresolvable problems largely caused by poor installation practices. These include earthing faults, which are very common with electromagnetic meters, and unreported damage to the meter during installation.
Buried meters should be assessed by the Agency for compliance with the above conditions. Where the conditions have not been met there is a risk that the meter is producing inaccurate data. In these cases the Agency should agree a programme with the licence holder to replace the meter(s). The rate and urgency of replacement will be a local operational decision, and will be proportionate to the costs and benefits of ensuring that the meter is recording abstractions accurately. This will vary according to the estimated inaccuracy of the existing meter, the potential environmental impacts of the abstraction and the costs associated with its replacement.

6.6 Verification of data transmission and recording

For instruments with an electronic output to an automatic data logging system or remote totaliser, it is important to verify that the signal reaching the logger or totaliser is correct. Each abstraction meter should have an individual readout so that its accuracy can be checked independently. Several readouts aggregated at a remote site will not necessarily give an accurate total abstraction from all sources. There are two approaches to this, either a known signal is imposed onto the transmission line at the meter end and checked on the logger display, an oscilloscope or a multimeter or the signal being generated by the instrument is measured simultaneously at the instrument output and at the logger. Note that some electronic meters incorporate a current or pulse generator which can be set to a known value for this purpose.

Injecting a known signal, calculating the expected reading for that signal and comparing that with what is actually shown is a useful way of detecting errors in the set up of the instrument, for example a wrong span setting or 0-20mA output selected instead of 4-20mA.

Regular comparisons should be made between an instrument’s internal totaliser (where fitted) or the local display and the values recorded on the logger. This should be undertaken at a minimum frequency of every 24 months for electromagnetic meters and more frequently for other types. The flowmeter output should be within ±2% of the known input signal.

The equipment used for these tests should be traceably calibrated. This can be done by a specialist laboratory.

6.7 Remedial action

If the flow check shows that the meter is outside specification, i.e. if at one or more points within its operating range, the error is greater than that permitted, then some remedial action will be necessary. There are two possibilities:

1. The meter is faulty, or
2. One or more aspects of the installation or site conditions are causing an error.

It is usually preferable to eliminate the second possibility before condemning the meter and requiring the abstractor to bear the cost of removing and replacing or repairing the meter. The information given in Sections 4, 5 and Appendix B may help. Particular conditions to look for are shown in Table 6.6 with possible courses of action. Site conditions will determine the most appropriate course in each case.
Table 6.6 - Remedial actions

<table>
<thead>
<tr>
<th>Problem</th>
<th>Possible courses of action</th>
</tr>
</thead>
<tbody>
<tr>
<td>pipe not running full</td>
<td>resite meter</td>
</tr>
<tr>
<td></td>
<td>reconfigure pipework (see Section 5.1.5)</td>
</tr>
<tr>
<td>meter installed in an unsuitable orientation</td>
<td>resite meter</td>
</tr>
<tr>
<td></td>
<td>reconfigure pipework</td>
</tr>
<tr>
<td></td>
<td>replace meter</td>
</tr>
<tr>
<td>Vibration in the pipe</td>
<td>secure pipework and meter</td>
</tr>
<tr>
<td></td>
<td>fit rubber couplings (see Section 5.3.3)</td>
</tr>
<tr>
<td>sources of flow disturbance nearby</td>
<td>resite meter (see Section 5.1.2)</td>
</tr>
<tr>
<td></td>
<td>fit flow straightener</td>
</tr>
<tr>
<td>radio or electromagnetic interference from nearby cables, e.g. overhead power lines or power lines to pumping equipment.</td>
<td>resite meter</td>
</tr>
<tr>
<td></td>
<td>screen meter or cables</td>
</tr>
<tr>
<td>wrongly sized meter running at the bottom of its range</td>
<td>replace meter (see Section 3.2)</td>
</tr>
<tr>
<td>poor coupling for ultrasonic transducers</td>
<td>re-install transducers</td>
</tr>
<tr>
<td>Inadequate earthing on electromagnetic devices</td>
<td>re-install all earthing connections</td>
</tr>
</tbody>
</table>

If such factors have been eliminated or the meter is visibly damaged, e.g. jerky register, severe corrosion or mechanical damage, then the abstractor has the responsibility to have it cleaned, repaired or replaced. This will usually involve removing the meter from the line. This may give a clearer indication of the problem and hence the action needed.

Mechanical meters will usually go out of specification at the low ends of their range first due to wear and require refurbishment. With many smaller sized meters, 100mm or less, replacement will be the most economic course.

To ensure that the meter performs correctly, repair or refurbishment should be carried out by an approved agent, qualified technician, or the manufacturer. A laboratory re-calibration may also be necessary.

Software is becoming available that will allow meters and their installations to be checked without full access being necessary. The system is based on the use of insertion probes and industry-established calculations for disturbances in the pipe and will give an uncertainty figure for the meter based on what is known about its installation and accuracy.
REFERENCES AND BIBLIOGRAPHY


6. EMC Directive 89/336/EEC.

OTHER USEFUL TEXTS


Spitzer, DW (1991) Flow Measurement. ISA.

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APPENDIX A - FLOW CONVERSION TABLES

1. Volume

1 litre (l) = 0.220 UK gallons
1 megalitre (Ml) = 1 000 000 litres
1 cubic metre (m³) = 1000 litres
1 UK gallon = 4.546 litres
1 US gallon = 3.385 litres

2. Volumetric flow rate

<table>
<thead>
<tr>
<th>Megalitres per day (Ml/day)</th>
<th>Cubic metres per hour (m³/h)</th>
<th>Gallons per minute (gall/min)</th>
<th>Litres per minute (l/min)</th>
<th>Litres per second (l/s)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.0</td>
<td>41.667</td>
<td>152.759</td>
<td>694.444</td>
<td>11.574</td>
</tr>
<tr>
<td>0.02400</td>
<td>1.0</td>
<td>3.666</td>
<td>16.667</td>
<td>0.278</td>
</tr>
<tr>
<td>0.00655</td>
<td>0.273</td>
<td>1.0</td>
<td>4.546</td>
<td>0.076</td>
</tr>
<tr>
<td>0.00144</td>
<td>0.060</td>
<td>0.220</td>
<td>1.0</td>
<td>0.017</td>
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<tr>
<td>0.08640</td>
<td>3.6</td>
<td>13.198</td>
<td>60.0</td>
<td>1.0</td>
</tr>
</tbody>
</table>

3. Pressure

<table>
<thead>
<tr>
<th>Bar (bar)</th>
<th>Standard atmosphere (atm)</th>
<th>Metres head of water (m H₂O)</th>
<th>Feet head of water (ft H₂O)</th>
<th>Pound force per sq. in. (psi)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.0</td>
<td>0.987</td>
<td>10.197</td>
<td>33.456</td>
<td>14.504</td>
</tr>
<tr>
<td>1.013</td>
<td>1.0</td>
<td>10.332</td>
<td>33.899</td>
<td>14.696</td>
</tr>
<tr>
<td>0.098</td>
<td>0.097</td>
<td>1.0</td>
<td>3.281</td>
<td>1.423</td>
</tr>
<tr>
<td>0.030</td>
<td>0.030</td>
<td>0.305</td>
<td>1.0</td>
<td>0.434</td>
</tr>
<tr>
<td>0.069</td>
<td>0.068</td>
<td>0.703</td>
<td>2.307</td>
<td>1.0</td>
</tr>
</tbody>
</table>
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APPENDIX B - EXISTING INSTALLATION ASSESSMENT

The following is a checklist of questions which might be asked when assessing a metering installation for compliance with the licence. This is a general list and not all questions will be applicable to all abstractions. References to relevant section numbers in this manual are given in brackets. A form is also included which might be helpful in recording the appropriate details.

The meter:

Meter type/model/serial number. Cross reference serial number and its location with the maintenance and licence records.

Meter installation date/meter age?

Is the meter correctly sized for the flow rates likely to be encountered? (See Section 3.2) Check manufacturer’s specification if available

Is the meter of an appropriate technology for the application? (See Section 4.1)

Does the meter record in metric or Imperial units?

Does it record in appropriately sized units? (See Section 4.12)

Is there any ancillary equipment, e.g. pulse unit, remote totaliser, logger, telemetry link? (See Section 4.12)

General condition of the meter.

Is the dial on the register going around smoothly? Is it jerky or noisy? Unless there is gross damage evident, it is difficult to tell much about the internal condition of a meter from the outside. On mechanical meters, excessive noise or a jerky dial indicates that there may be damage to the internal mechanism of the meter and it is likely to be outside specification.

On mechanical meters, is there any evidence of condensation/leakage in the register? (See Section 5.3.3)

Is there any evidence of tampering, e.g. broken seals?

On mechanical meters, are the counter figures aligned? Misalignment may indicate tampering in a similar way to a car odometer.

Do any parts of the meter look to have been replaced?

What means are in place to protect the meter reading? (See Section 3.4)

Is the meter the normal duty meter for that abstraction or a stand-by? If a stand-by, where is the duty meter?
**Meter installation**

Is the meter fitted with flow in the direction of the arrow on the meter body? (See Section 5.2.1)

On vertical installations, is the flow upwards through the meter? (See Section 5.1.4)

With electromagnetic meters, are the earthing links attached securely and correctly? (See Section 4.7)

Is the meter protected from frost? (See Section 5.3.3)

Are there sufficient up and downstream straight, unobstructed, rigid pipe lengths between the meter and any fittings? (See Section 5.1.2)

How far is the meter from any pump? (See Section 5.1.2)

Is the meter downstream of the pump? (See Section 5.1.2)

Is the installation such that the meter is kept full of water? (See Section 5.1.5)

Is the meter fitted with a non-return valve or disc type reverse flow restriction device? (See Section 5.2.1)

How is the flow through the meter regulated?

Is the regulation valve downstream of the meter?

Is there any air in the line? (See Section 5.1.5)

Is a strainer fitted? (See Section 5.3.5)

Is there evidence of leakage between the source and the meter?

Are there any unmetered take-off’s between source and meter?

Are any tappings between source and meter locked off, such that the meter cannot be by-passed? (See Section 3.4)

Do any joints or tappings show signs of recent use, e.g. shiny threads, which may indicate that the meter has been removed or by-passed?

Does the installation meet with Health and Safety requirements? (See Section 5.3.6)

Is there any heavy plant/switch gear/overhead power cable nearby which may cause interference to the meter? (See Section 5.3.4)
The source:

What type of source is it? (See Section 3.3)

Does the water being measured contain any weeds/gravel/sand or other debris? (See Section 3.3.1)

Is the water acidic/corrosive/low conductivity? (See Section 3.3.1)

Site records:

Is the meter included in the station maintenance schedule? (See Section 3.5.1)

When was any maintenance or replacement last carried out on the meter? (See Section 3.5.1)

Have any parts, particularly the register, been replaced? If so, when?

When was the meter last flow checked? (See Section 6)

Are all calibration/conformance certificates available? (See Section 6.1)

When was the meter last inspected?

How often is the meter read (logger downloaded) and by who?

Where are the records kept and in what format?

Do the patterns of abstraction meet what would be expected from experience of other similar installations?
# FLOW METER INSTALLATION INSPECTION FORM

<table>
<thead>
<tr>
<th>DATE OF INSPECTION:</th>
<th>INSPECTING OFFICER:</th>
</tr>
</thead>
<tbody>
<tr>
<td>LICENCE NUMBER:</td>
<td>CONTACT:</td>
</tr>
<tr>
<td>LICENCE HOLDER</td>
<td></td>
</tr>
<tr>
<td>ADDRESS:</td>
<td>SITE ADDRESS (IF DIFFERENT):</td>
</tr>
</tbody>
</table>

**LOCATION OF METER:**

**METER DETAILS**

- **TYPE:**
- **MAKE:**
- **MODEL:**
- **READING:**
- **UNITS:**
- **SERIAL NO.:**
- **DATE INSTALLED:**
- **PIPE DIAMETER:**
- **VISIBLE DAMAGE:** Y/N IF YES DESCRIBE:
- **CONDENSATION:** Y/N
- **DIAL/COUNTER OPERATION SMOOTH:** Y/N

**INSTALLATION**

- **UPSTREAM LENGTHS STRAIGHT PIPE:** m  SUFFICIENT FOR METER TYPE: Y/N
- **DOWNSTREAM LENGTHS STRAIGHT PIPE:** m  SUFFICIENT FOR METER TYPE: Y/N
- **DISTANCE FROM PUMP:** m
- **PIPE FULL:** Y/N  NON-RETURN VALVE FITTED: Y/N
- **FLOW DIRECTION CORRECT:** Y/N  FLOW UPWARDS IN VERTICAL PIPE: Y/N
- **CAN METER BE BY-PASSED:** Y/N  ANY LEAKAGE BETWEEN SOURCE AND METER: Y/N
- **DEBRIS IN WATER:** Y/N  STRAINER FITTED: Y/N  FROST PROTECTION: Y/N
- **IS WATER ACIDIC:** Y/N  CORROSIVE: Y/N  LOW CONDUCTIVITY: Y/N

**RECORDS**

- **METER CALIBRATED:** Y/N  DATE:
- **CERTIFICATE AVAILABLE:** Y/N
- **MAINTENANCE:** Y/N  FREQUENCY:
- **WHO BY:**
- **READINGS TAKEN:** Y/N  FREQUENCY:
- **WHO BY:**  WHERE KEPT:
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APPENDIX C - PHOTOGRAPHS OF FLOWMETERS AND INSTALLATIONS
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Plate 1 Venturi meter installation
Note the signal cable coming from the pulse output module beneath the register. A seal, in the form of a copper wire with a lead seal, links the pulse unit to the meter body in order to improve security.
Plate 5 ABB Kent-Taylor Magmaster electromagnetic flowmeter (1995)

Note rubber coupling upstream (right) to eliminate pipe vibration. The accuracy of this particular meter may be impaired by the reducing cones either side.
This portable meter can be used for in-situ checks. The transducers are mounted on the rail strapped to the side of the pipe. Data on the installation such as pipe bore, material and pipe wall thickness, are programmed into the instrument which then calculates the optimum spacing for the transducers.
Plate 7 Installation example 1 (Poor).

Flow enters through the grey pipe in the bottom left of the picture, goes through two right angled bends before the T piece where there is an unmetered take off (the yellow hose). The flow splits at the second T piece. Some goes up around another bend then immediately through the Helix meter. A further bend is installed immediately on the outlet of the meter. The rest of the flow passes around a by-pass which is not metered.
Flow is right to left through the Helix meter. The meter should be 5D downstream of the long radius bend. The large pipe operated by the red handled valve clearly by-passes the meter.
Plate 11 Installation example 5 (Poor)
This Helix meter is too close to the pump. It is a 100mm meter and hence there should be 2m of straight pipe between it and the pump. It is also unsupported and hence all its weight is being carried by the clamp fitting upstream.
Plate 12 Installation example 6 (Poor)

Helix meter is installed too close to the T upstream and the NRV (non return valve) downstream.
Plate 13 Installation example 7 (Poor)
Helix meter installed too close to the pump and NRV upstream and the T and valve downstream.
There are adequate up and downstream lengths on this electromagnetic meter but the Earthing ties are hanging loose and have not been connected to the pipe.
Plate 16 Installation example 2 (Good)

This is a spray irrigation installation with adequate up and downstream lengths on the meter. The pipework to the right of the picture slopes uphill ensuring that the meter stays full.
## SUPPLIERS OF FLOWMETERS

This list is not intended to be a recommendation of those companies listed. The manufacturer or supplier should be consulted regarding the suitability of any meter for a particular purpose. Every effort has been made to ensure that the information given in this table is accurate at the time of publication (2002) however it is not intended to be a comprehensive list of all suppliers.

Small mechanical meters, up to 100mm, may be readily available from local agricultural or plumbing suppliers. Officers may also wish to hold lists of suppliers in their own region.

<table>
<thead>
<tr>
<th>Company</th>
<th>Types supplied</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>Abako Ltd.</strong></td>
<td>✓ ✓</td>
</tr>
<tr>
<td>102 Bromham Road, Biddenham, Bedford, MK40 4AH</td>
<td>✓ ✓</td>
</tr>
<tr>
<td>Tel: 01234 353353 Fax: 01234 349719</td>
<td>✓ ✓</td>
</tr>
<tr>
<td><strong>ABB Automation</strong></td>
<td>✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ *</td>
</tr>
<tr>
<td>Oldends Lane, Stonehouse, Glos, GL10 3TA</td>
<td>✓ ✓ ✓ ✓ ✓ ✓ ✓</td>
</tr>
<tr>
<td>Tel: 01453 826661 Fax: 01453 827856 <a href="http://www.abb.co.uk">www.abb.co.uk</a></td>
<td>✓ ✓ ✓ ✓ ✓ ✓ ✓</td>
</tr>
<tr>
<td><strong>ABB Metering Ltd.</strong></td>
<td>✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓</td>
</tr>
<tr>
<td>Lea Works, Pondwicks Road, Luton, LU1 3LJ</td>
<td>✓ ✓ ✓ ✓ ✓ ✓ ✓</td>
</tr>
<tr>
<td>Tel: 01582 402020 Fax: 01582 438051 <a href="http://www.abb.co.uk">www.abb.co.uk</a></td>
<td>✓ ✓ ✓ ✓ ✓ ✓ ✓</td>
</tr>
<tr>
<td><strong>Able Instruments &amp; Controls Ltd.</strong></td>
<td>✓ ✓ ✓ ✓ ✓</td>
</tr>
<tr>
<td>Cutbush Park, Danehill, Lower Earley, Reading, Berkshire, RG6 4UT</td>
<td>✓ ✓ ✓ ✓ ✓</td>
</tr>
<tr>
<td>Tel: 0118 916 9530 Fax: 0118 931 2161 <a href="http://www.able.co.uk">www.able.co.uk</a></td>
<td>✓ ✓ ✓ ✓ ✓</td>
</tr>
<tr>
<td><strong>Acal Auriema Ltd.</strong></td>
<td>✓ ✓ ✓ ✓ ✓</td>
</tr>
<tr>
<td>442 Bath Road, Slough, Berks, SL1 6BB</td>
<td>✓ ✓ ✓</td>
</tr>
<tr>
<td>Tel: 01628 604353 Fax: 01628 603730 <a href="http://www.acal-auriema.co.uk">www.acal-auriema.co.uk</a></td>
<td>✓ ✓ ✓</td>
</tr>
<tr>
<td><strong>Access Instrumentation Ltd.</strong></td>
<td>✓ ✓ ✓ ✓ ✓</td>
</tr>
<tr>
<td>The Centre, Reading Road, Eversley, Hants, RG27 0NB</td>
<td>✓ ✓ ✓</td>
</tr>
<tr>
<td>Tel: 0118 973 4702 Fax: 0118 973 1177 <a href="http://www.accessinstrumentation.co.uk">www.accessinstrumentation.co.uk</a></td>
<td>✓ ✓ ✓</td>
</tr>
<tr>
<td><strong>Actaris Metering Systems</strong></td>
<td>✓ ✓ ✓ ✓ ✓ ✓ ✓</td>
</tr>
<tr>
<td>PO Box 3, Talbot Road, Stretford, Manchester, M32 0XX</td>
<td>✓ ✓ ✓</td>
</tr>
<tr>
<td>Tel: 0161 865 1181 Fax: 0161 954 4902 <a href="http://www.actaris.com">www.actaris.com</a></td>
<td>✓ ✓ ✓</td>
</tr>
</tbody>
</table>

Key to types: 1 Primary d.p. elements, 2 d.p. cells, 3 Rotary piston, 4 Woltmann turbines, 5 Irrigation, 6 Electromagnetic, 7 Ultrasonic (clamp-on), 8 Ultrasonic (wetted), 9 Insertion, 10 Jet, C Calibration services * indicates UKAS accredited
<table>
<thead>
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<th>Types supplied</th>
</tr>
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<tr>
<td>Akro Valve Co.</td>
<td>✓</td>
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<tr>
<td>Unit 2, Chaucer Industrial Estate, Dittons Road, Polegate, East Sussex, BN26 6JF Tel: 01323 485272 Fax: 01323 485273 <a href="http://www.akrovalve.co.uk">www.akrovalve.co.uk</a></td>
<td>✓</td>
</tr>
<tr>
<td>Albion Distribution Ltd.</td>
<td>✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓</td>
</tr>
<tr>
<td>Fallbank Industrial Estate, Dodworth, Barnsley, South Yorkshire, S75 3LS Tel: 01226 729900 Fax: 01226 288011</td>
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<tr>
<td>Altecnic</td>
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<tr>
<td>Airfield Industrial Estate, Hixon, Staffs, ST18 0PF Tel: 01889 207200 Fax: 01889 270577 <a href="http://www.altecnic.co.uk">www.altecnic.co.uk</a></td>
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<tr>
<td>Apollo Flow Measurement Ltd.</td>
<td>✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓</td>
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<tr>
<td>2 Bentley Lane Industrial Park, Bentley Lane, Walsall, WS2 8TL Tel: 01922 645647 Fax: 01922 640326</td>
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<tr>
<td>Arkon Flow Systems</td>
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<tr>
<td>Record House, Atlantic Street, Altrincham, Cheshire, WA14 5DB Tel: 0161 928 6211 Fax: 0161 926 9750 <a href="http://www.arkon.co.uk">www.arkon.co.uk</a></td>
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<td>Buhler Montec Group Ltd.</td>
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<tr>
<td>Pacific Way, Salford, Manchester, M5 2DL Tel: 0161 872 1487 Fax: 0161 848 7324 <a href="http://www.buhlermontec.co.uk">www.buhlermontec.co.uk</a></td>
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<td>Burkert Contromatic Ltd.</td>
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<td>Brimscombe Port Business Park, Brimscombe, Stroud, Glos. GL5 2QF Tel: 01453 731353 Fax: 01453 731343 <a href="http://www.burkert-contromatic.co.uk">www.burkert-contromatic.co.uk</a></td>
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<tr>
<td>Coulton Instrumentation Ltd.</td>
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<tr>
<td>17 Somerford Business Park, Christchurch, Dorset, BH23 3RU Tel: 01202 480303 Fax: 01202 480808 <a href="http://www.coulton.com">www.coulton.com</a></td>
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<td>Dales Water Services Ltd.</td>
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<tr>
<td>Witherick Lane, Melmerby, Ripon, North Yorkshire, HG4 5JB Tel: 01765 603043 Fax: 01765 607078 <a href="http://www.daleswater.co.uk">www.daleswater.co.uk</a></td>
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**Key to types:** 1 Primary d.p. elements, 2 d.p. cells, 3 Rotary piston, 4 Woltmann turbines, 5 Irrigation, 6 Electromagnetic, 7 Ultrasonic (clamp-on), 8 Ultrasonic (wetted), 9 Insertion, 10 Jet, C Calibration services * indicates UKAS accredited
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<td>Magfio House, Ebley Road, Stonehouse, Gloucestershire, GL10 2LU Tel: 01453 828891 Fax: 01453 824013 <a href="http://www.danfoss.com">www.danfoss.com</a></td>
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<td>Fisher-Rosemount Limited, Horsfield Way, Bredbury Industrial Estate, Stockport, SK6 2SU Tel: 0161 430 7100 Fax: 0161 494 5328 <a href="http://www.emersonprocess.com">www.emersonprocess.com</a></td>
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<td>11a Shenley Road, Borehamwood, Hertfordshire, WD6 1AD Tel: 0208 207 6565 Fax: 0208 207 3082 <a href="http://www.flowline.co.uk">www.flowline.co.uk</a></td>
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<td>Manor Royal, Crawley, West Sussex, RH10 2SJ Tel: 01293 526000 Fax: 01293 541312 <a href="http://www.foxboro.com">www.foxboro.com</a></td>
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<td>Paradise Way, Coventry, CV2 2ST Tel: 02476 535535 Fax: 02476 530450 <a href="http://www.georgefischer.co.uk">www.georgefischer.co.uk</a></td>
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<td>Honeywell House, Arlington Business Park, Bracknell, Berks, RG12 1EB Tel: 01344 656000 Fax: 01344 656240 <a href="http://www.iac.honeywell.com">www.iac.honeywell.com</a></td>
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<td>Instrument House, Woodward Road, Knowsley Industrial Park, Liverpool, L33 7UZ Tel: 0151 546 4943 Fax: 0151 548 6262 <a href="http://www.itiuk.com">www.itiuk.com</a></td>
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## Equipment suppliers

### Abstraction Metering Good Practice Manual

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<th>Company</th>
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<td><strong>Invensys Metering Systems Ltd.</strong></td>
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<td>Davenport House, Davenport Gate, West</td>
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<td>Portway Industrial Estate, Andover, Hants, SP10 3SQ</td>
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<tr>
<td>Tel: 01264 336223 Fax: 01264 336870</td>
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<tr>
<td><a href="http://www.ims.invensys.com">www.ims.invensys.com</a></td>
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<tr>
<td><strong>Katronic Technologies</strong></td>
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<tr>
<td>23 Cross Street, Leamington Spa, Warwickshire, CV32 4PX</td>
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</tr>
<tr>
<td>Tel: 01926 882954 Fax: 01926 338649</td>
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<td><a href="http://www.katronic.co.uk">www.katronic.co.uk</a></td>
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<td><strong>Kobold Instruments</strong></td>
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<tr>
<td>Kobold House, 8-9 Brunts Business Centre, Samuel Brunts Way,</td>
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<tr>
<td>Mansfield, Nottingham, NG18 2AH</td>
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<tr>
<td>Tel: 01623 427701 Fax: 01623 427702</td>
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<td><a href="http://www.koboldusa.com">www.koboldusa.com</a></td>
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<td><strong>Krohne Ltd.</strong></td>
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<td>Northants, NN8 6AE</td>
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<td>Tel: 01933 408500 Fax: 01933 408501</td>
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<td>Bucks, HP19 3RS</td>
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<tr>
<td>Tel: 01296 420341 Fax: 01296 436446</td>
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<td><a href="http://www.litremeter.com">www.litremeter.com</a></td>
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<td><strong>J Llewlin and Co.</strong></td>
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<td>Trewarren Farm, St Ishmaels, Haverfordwest, Pembrokeshire, SA</td>
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<td>Tel: 01646 636260 Fax: 01646 636410</td>
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<td>Tel: 01628 810456 Fax: 01628 531540</td>
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<td><a href="http://www.micronicsltd.co.uk">www.micronicsltd.co.uk</a></td>
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<td><strong>Nixon Flowmeters Ltd.</strong></td>
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<td>Tel: 01242 243006 Fax: 01242 222487</td>
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<td><strong>Norstrom Normanner Group Ltd.</strong></td>
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<td>Tel: 01633 489479 Fax: 01633 877857 <a href="http://www.palmer.co.uk">www.palmer.co.uk</a></td>
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<td>40 Upper Mulgrave Road, Cheam, Surrey, SM2 7AJ</td>
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<td><strong>Phoenix Flow Measurement Ltd.</strong></td>
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<td>Enterprise House, 2 Cambridge Road, Kingston upon Thames, Surrey, KT1 3JU</td>
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<td>Tel: 020 8547 0331 Fax: 020 8547 0332 <a href="http://www.badgermeter.de">www.badgermeter.de</a></td>
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<td><strong>The Ranger Instrument Co. Ltd.</strong></td>
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<td>Tel: 01256 464911 Fax: 01256 464366 <a href="http://www.bayham.demon.co.uk">www.bayham.demon.co.uk</a></td>
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<td><strong>Reliance Water Controls Ltd.</strong></td>
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<td><strong>Roxspur Measurement &amp; Control Ltd.</strong></td>
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### Key to types:

1. Primary d.p. elements
2. d.p. cells
3. Rotary piston
4. Woltmann turbines
5. Irrigation
6. Electromagnetic
7. Ultrasonic (clamp-on)
8. Ultrasonic (wetted)
9. Insertion
10. Jet
C. Calibration services
* indicates UKAS accredited
METER CALIBRATION SERVICES

This list is not intended to be a recommendation of those companies listed. Every effort has been made to ensure that the information is accurate at the time of publication (2002) however it is not intended to be a comprehensive list of all suppliers.

CALIBRATION LABORATORIES

Many suppliers and manufacturers have their own calibration facilities or are able to arrange meter checking and calibration on other facilities. Those with their own facilities are indicated in the tables of meter suppliers. Some independent meter testing laboratories are shown below. Those marked with an asterisk have UKAS accreditation for flowmeter calibration on cold water. Users should check the scope of the accreditation against their requirements.

AEMS
The Energy Centre, Finnimore Industrial Estate, Ottery St. Mary, Devon, EX11 1NR
Tel: 01404 812294 Fax: 01404 812603
Website: www.yatesmeter.co.uk e-mail: info@yatesmeter.co.uk

Foxwell Instruments
Crown House, Kings Road, Evesham, WR11 5BE
Tel: 01386 446255 Fax: 01386 421991
Website: freespace.virgin.net/foxwell.instruments e-mail: foxwell.instruments@virgin.net

Heap and Partners Ltd.
Rallim House, Carham Road, Carr Lane Industrial Estate, Hoylake, Wirral, L47 4FF
Tel: 0151 632 3271 Fax: 0151 632 4128
Website: www.heaps.co.uk e-mail: info@heaps.co.uk

National Engineering Laboratory*
Flow Centre, East Kilbride, Glasgow, G75 0QU
Tel: 01355 220222 Fax: 01355 272999
Website: www.nel.uk e-mail: info@nel.uk

Powergen*
Power Technology Plant Test, Faradaway Avenue, Hams Hall Distribution Park, Coleshill, Birmingham, B46 1PT
Tel: 0121 607 2270 Fax: 0121 607 2275
Website: www.powertech.co.uk

Sira Test and Certification Ltd
South Hill, Chislehurst, Kent, BR7 5EH
Tel: 0208 4672636 Fax: 0208 2953005
Website: www.sirateservices.com e-mail: sales@siratec.co.uk

WRc-NSF*
Fern Close, Pen-y-Fan Industrial Estate, Oakdale, Gwent NP1 4EH
Tel: 01495 248454 Fax: 01495 249234
Website: www.wrcetc.co.uk e-mail: wrcetc@wrcplc.co.uk

IN-SITU VERIFICATIONS
AEMS
The Energy Centre, Finnimore Industrial Estate, Ottery St. Mary, Devon, EX11 1NR
Tel: 01404 812294    Fax: 01404 812603
Website: www.yatesmeter.co.uk    e-mail: info@yatesmeter.co.uk

Bestobell Service
158 Edinburgh Avenue, Slough, Berks, SL1 4UE
Tel: 01753 756600    Fax: 01753 823589
Website: www.solartronmobrey.com    e-mail: service@solartron.com

Bestobell Service also have local offices in Birmingham (Tel: 0121 730 1900), Stockport (Tel: 0161 483 0931), Batley (Tel: 01924 441960), and Gravesend (Tel: 01474 355976).

Hydroserve Flow Measurement
97 Front Street, Whickham, Newcastle upon Tyne, NE16 4JL
Tel: 0191 4961249    Fax: 0191 4881877
Website: www.hydroserveuk.com    e-mail: home@hydroserveuk.com

R S Hydro Ltd.
4 Fleetwood Avenue, Powick, Worcestershire, WR2 4PY
Tel: 01905 830627    Fax: 01905 830627
Website: www.rs-hydro.co.uk    e-mail: info@rs-hydro.co.uk

SGS United Kingdom Ltd.
Rossmore Business Park, Ellesmere Port, South Wirral, CH65 3EN
Tel: 0151 350 6666    Fax: 0151 350 6600
Website: www.sgs.co.uk    e-mail: ukenquiries@sgsgroup.com

WRc plc
Frankland Road, Blagrove, Swindon, Wilts, SN5 8YF
Tel: 01793 865000    Fax: 01793 865001
Website: www.wrecplc.co.uk    e-mail: solutions@wrecplc.co.uk